

Environmental Noise Impact Assessment for the Ammonia Terminal, Walvis Bay North Port Area

Project done for Environmental Compliance Consultancy

Report Compiled By:
Reneé von Gruenewaldt

Report No: 24ECC04 | **Date:** November 2024



Address: 62 Constantia Ave, Pretoria
Postal: PostNet Suite #18 Private Bag x59, Halfway House, 1685
Tel: +27 (0)11 805 1940
www.airshed.co.za

Report Details

Report Title	Environmental Noise Impact Assessment for the Ammonia Terminal, Walvis Bay North Port Area
Client	Environmental Compliance Consultancy (Pty) Ltd
Report Number	24ECC04
Report Version	Rev 3
Date	November 2024
Prepared by	Reneé von Gruenewaldt (Pr. Sci. Nat), MSc (University of Pretoria)
Reviewed by	Nick Grobler BEng (Chem), BEng (Hons) (Env), (University of Pretoria)
Notice	Airshed Planning Professionals (Pty) Ltd is a consulting company located in Midrand, South Africa, specialising in (1) air quality impact assessments and (2) environmental noise impact assessments. The company originated in 1990 as Environmental Management Services, which amalgamated with its sister company, Matrix Environmental Consultants, in 2003.
Declaration	Airshed is an independent consulting firm with no interest in the project other than to fulfil the contract between the client and the consultant for delivery of specialised services as stipulated in the terms of reference.
Copyright Warning	Unless otherwise noted, the copyright in all text and other matter (including the manner of presentation) is the exclusive property of Airshed Planning Professionals (Pty) Ltd. It is a criminal offence to reproduce and/or use, without written consent, any matter, technical procedure and/or technique contained in this document.

Revision Record

Version	Date	Comments
Rev 0	October 2024	For internal review
Rev 1	October 2024	For client review
Rev 2	November 2024	Incorporation of client's comments
Rev 3	November 2024	Incorporation of client's comments

Glossary and Abbreviations

BSI	British Standards Institution
dB	Descriptor that is used to indicate 10 times a logarithmic ratio of quantities that have the same units, in this case sound pressure.
dBA	Descriptor that is used to indicate 10 times a logarithmic ratio of quantities that have the same units, in this case sound pressure that has been A-weighted to simulate human hearing.
ECC	Environmental Compliance Consultancy
EHS	Environmental, Health, and Safety (IFC)
Hz	Frequency in Hertz
IA	Instrument Air
IEC	International Electro Technical Commission
IFC	International Finance Corporation
ISO	International Standards Organisation
Kn	Noise propagation correction factor
K1	Noise propagation correction for geometrical divergence
K2	Noise propagation correction for atmospheric absorption
K3	Noise propagation correction for the effect of ground surface;
K4	Noise propagation correction for reflection from surfaces
K5	Noise propagation correction for screening by obstacles
km	Kilometre
L_{Aeq} (T)	The A-weighted equivalent sound pressure level, where T indicates the time over which the noise is averaged (calculated or measured) (in dBA)
L_{Aleq} (T)	The impulse corrected A-weighted equivalent sound pressure level, where T indicates the time over which the noise is averaged (calculated or measured) (in dBA)
L_{A90}	The A-weighted 90% statistical noise level, i.e. the noise level that is exceeded during 90% of the measurement period. It is a very useful descriptor which provides an indication of what the L _{Aeq} could have been in the absence of noisy single events and is considered representative of background noise levels (L _{A90}) (in dBA)
L_{AFmax}	The A-weighted maximum sound pressure level recorded during the measurement period
L_{AFmin}	The A-weighted minimum sound pressure level recorded during the measurement period
L_p	Sound pressure level (in dB)
Ltd	Limited
L_w	Sound Power Level (in dB)
m	Metres
m³	Cubic metres
m/s	Speed in metres per second
N₂	Nitrogen

N/A	Not applicable
NACA	National Association for Clean Air
NSR	Noise sensitive receptor
p	Pressure in Pa
Pa	Pressure in Pascal
μPa	Pressure in micro-pascal
p_{ref}	Reference pressure, 20 μPa
PSVs	Pressure safety valves
Pty	Proprietary
SABS	South African Bureau of Standards
SACNASP	South African Council for Natural Scientific Professions
SANS	South African National Standards
SLM	Sound Level Meter
tph	Tonnes per hour
WRF	Weather Research and Forecasting
°C	Degrees Celsius

Executive Summary

Cleanergy Solutions Namibia Pty Ltd is intending on becoming a driving force in the growth of the Namibia's hydrogen economy, while contributing to the global shift for industrial decarbonisation. To this end, Cleanergy Solutions intends to use the abundant sun to produce hydrogen and then combine the hydrogen with nitrogen to produce ammonia for exportation purposes. The proposed activities consist of a hydrogen pipeline starting near Arandis to the ammonia facility on Farm 58, close to Walvis Bay. Three routes have been proposed. From the ammonia facility, ammonia is transported to an ammonia tank located north of Walvis Bay. From this ammonia storage tank, ammonia will be exported via a ship.

Separate environmental authorizations have been applied for the hydrogen pipeline and the ammonia plant and pipeline. This assessment focuses on the ammonia terminal and its associated impacts.

Airshed Planning Professionals (Pty) Ltd was commissioned by Environmental Compliance Consultancy (Pty) Ltd (ECC) to undertake an Environmental Noise Impact Assessment for the proposed ammonia terminal (hereafter referred to as the project).

The main objective of the noise specialist study was to determine the significance of impacts on the acoustic environment and noise receptors (NSRs) given noise generated by construction activities proposed for the project.

To meet the above objective, the following tasks were included in the Scope of Work:

1. A review of technical information for the operation of the project.
2. A review of the legal requirements and applicable environmental noise guidelines.
3. A study of the receiving (baseline) acoustic environment, including:
 - a. The identification of NSRs from available maps;
 - b. Analysis of sampled baseline noise levels.
4. An impact assessment, including:
 - a. A source inventory for the project.
 - b. Noise propagation simulations to determine environmental noise levels over the selected study area and at NSRs as a result of project activities.
 - c. The screening of simulated noise levels against environmental noise criteria.
5. The identification and recommendation of suitable noise management measures and monitoring requirements.
6. Determining impact significance.
7. The preparation of a comprehensive specialist environmental noise impact assessment report.

In the assessment of sampled and simulated noise levels, reference was made to the International Finance Corporation (IFC) noise level guidelines for residential, institutional and educational receptors (55 dBA during the day and 45 dBA during the night) since these are applicable to nearby NSRs. Annoyance was assessed according to the South African National Standard (SANS) 10103 (2008) scale.

The baseline acoustic environment was described in terms of the location of NSRs, the ability of the environment to attenuate noise over long distances, as well as existing baseline noise levels. The following was found:

- The closest potential sensitive receptors to the proposed project consist of the residential areas of Walvis Bay.
- The baseline noise levels (L_{Aeq}) just east of Walvis Bay during day- and night-time conditions was measured as 38.3 dBA and 42.2 dBA respectively.

A source inventory was developed for the project operations. A detailed list of equipment for operations was provided. Noise levels for the equipment were calculated using predictive equations for industrial machinery as per the Handbook of Acoustics, Chapter 69, by Bruce and Moritz (1998).

The source inventory and information on local land use were used to populate the noise attenuation model (CadnaA, ISO 9613). The propagation of noise was calculated over an area of 5 km east-west by 5 km north-south. The area was divided into a grid matrix with a 20 m resolution.

The following project scenarios were assessed:

- Normal project operations.
- Emergency project activities where there would be a worst-case scenario of flaring due to a sudden change in the ambient pressure. This would result in a maximum release from the tank pressure safety valves (PSVs) through the flare. It should be noted that this worst-case scenario is not a normal operating condition.
- Emergency project activities where the scrubber is off-line, and the throughput is redirected to the scrubber.
- Project commissioning activities.

The main findings of the impact assessment were as follows:

- (a) Exceedances of the IFC noise guideline for residential areas at the closest NSR to the project (i.e. Walvis Bay):
- Normal project operations:
 - Day-time: no exceedances of the IFC noise guideline for residential areas;
 - Night-time: no exceedances of the IFC noise guideline for residential areas;
 - Emergency project activities (where the ammonia release from the main PSVs on the tank are released through the flare for an hour):
 - Day-time: no exceedances of the IFC noise guideline for residential areas;
 - Night-time: simulated noise levels (53.2 dBA) exceed the IFC noise guideline (45 dBA) for residential areas;
 - Emergency project activities (scrubber not available and throughput released through the flare for an hour):
 - Day-time: no exceedances of the IFC noise guideline for residential areas;
 - Night-time: no exceedances of the IFC noise guideline for residential areas;
 - Project commissioning operations:

- Day-time: no exceedances of the IFC noise guideline for residential areas;
- Night-time: no exceedances of the IFC noise guideline for residential areas.

(b) Expected community reaction from Walvis Bay due to project activities:

- Normal project operations: no community reaction;
- Emergency project activities (where the ammonia release from the main PSVs on the tank are released through the flare for an hour): 'medium' community reaction with widespread complaints;
- Emergency project activities (scrubber not available and throughput released through the flare for an hour): no community reaction;
- Project commissioning operations: no community reaction.

Based on the findings of the assessment for normal project operations and provided the recommended general "good practice" management and mitigation measures are in place, it is the specialist opinion that the ammonia terminal may be authorised from an environmental noise perspective.

Table of Contents

1	INTRODUCTION.....	1
1.1	Study Objective	1
1.2	Scope of Work.....	1
1.3	Specialist Details	3
1.4	Background to Environmental Noise and the Assessment Thereof.....	3
1.5	Approach and Methodology.....	7
1.6	Management of Uncertainties.....	10
2	LEGAL REQUIREMENTS AND NOISE LEVEL GUIDELINES.....	11
2.1	International Finance Corporation Guidelines on Environmental Noise	11
2.2	SANS 10103 Guidance on Estimating Community Response.....	11
3	DESCRIPTION OF THE RECEIVING ENVIRONMENT	12
3.1	Noise Sensitive Receptors	12
3.2	Environmental Noise Propagation and Attenuation Potential	12
3.3	Noise Survey and Results	15
4	IMPACT ASSESSMENT	19
4.1	Process Description.....	19
4.2	Noise Sources and Sound Power Levels	20
4.3	Noise Propagation and Simulated Noise Levels.....	23
5	MANAGEMENT MEASURES	29
5.1	Controlling Noise at the Source	29
5.2	Monitoring.....	30
6	CONCLUSION	32
7	REFERENCES.....	33
	APPENDIX A – SPECIALIST CURRICULUM VITAE	34
	APPENDIX B – DECLARATION OF INDEPENDENCE.....	41
	APPENDIX C – SURVEY SITE PHOTOS.....	42
	APPENDIX D – TIME-SERIES, STATISTICAL, AND FREQUENCY SPECTRUM RESULTS.....	48

List of Tables

Table 2-1: IFC noise level guidelines	11
Table 3-1: Summary of noise measurements conducted in 2024	17
Table 4-1: Equipment list for the project	20
Table 4-2: Octave band frequency spectra L_w 's	22
Table 4-3: Calculated sound power levels for the flare	23
Table 4-4: Summary of simulated noise levels (provided as dBA) due to the proposed project activities at the closest NSR (Walvis Bay)	24

List of Figures

Figure 1-1: The proposed ammonia plant, ammonia terminal, and ammonia and hydrogen pipelines.....	2
Figure 1-2: The decibel scale and typical noise levels (Brüel & Kjær Sound & Vibration Measurement A/S, 2000)4	
Figure 1-3: A-weighting curve	5
Figure 3-1: Sensitive receptors within the study area and baseline noise survey sites.....	13
Figure 3-2: Wind rose for Walvis Bay (as obtained from WRF data) for the period 2021 to 2023.....	14
Figure 3-3: Bending the path of sound during typical day time conditions (image provided on the left) and night-time conditions (image provided on the right)	14
Figure 3-4: Topography for the study area.....	15
Figure 3-5: Day-time broadband survey results	16
Figure 3-6: Night-time broadband survey results	16
Figure 4-1: Simulated day-time noise levels due to normal project operations only	25
Figure 4-2: Simulated night-time noise levels due to normal project operations only	25
Figure 4-3: Simulated day-time noise levels due to project emergency process (assuming 1 hr tank PSVs maximum release through the flare)	26
Figure 4-4: Simulated night-time noise levels due to project emergency process (assuming 1 hr tank PSVs maximum release through the flare)	26
Figure 4-5: Simulated day-time noise levels due to project emergency process (assuming 1 hr Scrubber emission release through the flare)	27
Figure 4-6: Simulated night-time noise levels due to project emergency process (assuming 1 hr Scrubber emission release through the flare)	27
Figure 4-7: Simulated day-time noise levels due to project commissioning operations only.....	28
Figure 4-8: Simulated night-time noise levels due to project commissioning operations only.....	28
Figure C-1: Photographs of environmental noise Site 1.....	42
Figure C-2: Photographs of environmental noise Site 2.....	42
Figure C-3: Photographs of environmental noise Site 3.....	43
Figure C-4: Photographs of environmental noise Site 4.....	43
Figure C-5: Photographs of environmental noise Site 5.....	44
Figure C-6: Photographs of environmental noise Site 6.....	44
Figure C-7: Photographs of environmental noise Site 7.....	45
Figure C-8: Photographs of environmental noise Site 8.....	45
Figure C-9: Photographs of environmental noise Site 9.....	46
Figure C-10: Photographs of environmental noise Site 10.....	46
Figure C-11: Photographs of environmental noise Site 11.....	47
Figure C-12: Photographs of environmental noise Site 12.....	47
Figure D-1: Detailed day- and night-time survey results for Site 1	48
Figure D-2: Detailed day- and night-time survey results for Site 2	49
Figure D-3: Detailed day- and night-time survey results for Site 3	50
Figure D-4: Detailed day- and night-time survey results for Site 4	51
Figure D-5: Detailed day- and night-time survey results for Site 5.....	52

Figure D-6: Detailed day- and night-time survey results for Site 6	53
Figure D-7: Detailed day- and night-time survey results for Site 7	54
Figure D-8: Detailed day- and night-time survey results for Site 8	55
Figure D-9: Detailed day- and night-time survey results for Site 9	56
Figure D-10: Detailed day- and night-time survey results for Site 10	57
Figure D-11: Detailed day- and night-time survey results for Site 11	58
Figure D-12: Detailed day- and night-time survey results for Site 12	59

1 Introduction

Cleanergy Solutions Namibia Pty Ltd is intending on becoming a driving force in the growth of the Namibia's hydrogen economy, while contributing to the global shift for industrial decarbonisation. To this end, Cleanergy Solutions intends to use the abundant sun to produce hydrogen and then combine the hydrogen with nitrogen to produce ammonia for exportation purposes. The proposed activities consist of a hydrogen pipeline starting near Arandis to the ammonia facility on Farm 58, close to Walvis Bay. Three routes have been proposed, as indicated in Figure 1-1. From the ammonia facility, ammonia is transported to an ammonia tank located north of Walvis Bay. From this ammonia storage tank, ammonia will be exported via a ship.

Separate environmental authorizations have been applied for the hydrogen pipeline and the ammonia plant and pipeline. This assessment focuses on the ammonia terminal and its associated impacts.

Airshed Planning Professionals (Pty) Ltd was commissioned by Environmental Compliance Consultancy (Pty) Ltd (ECC) to undertake an Environmental Noise Impact Assessment for the proposed ammonia terminal (hereafter referred to as the project).

1.1 Study Objective

The main objective of the noise specialist study was to determine the significance of impacts on the acoustic environment and potential noise sensitive receptors (NSRs) given noise generated by activities proposed as part of the project.

1.2 Scope of Work

To meet the above objective, the following tasks were included in the Scope of Work:

1. A review of technical information for the project.
2. A review of the legal requirements and applicable environmental noise guidelines.
3. A study of the receiving (baseline) acoustic environment, including:
 - a. The identification of NSRs from available maps;
 - b. Analysis of sampled baseline noise levels.
4. An impact assessment, including:
 - a. A source inventory for project operations.
 - b. Noise propagation simulations to determine environmental noise levels over the selected study area and at NSRs as a result of the project operations.
 - c. The screening of simulated noise levels against environmental noise criteria.
5. The identification and recommendation of suitable noise management measures and monitoring requirements.
6. Determining impact significance.
7. The preparation of a comprehensive specialist environmental noise impact assessment report.

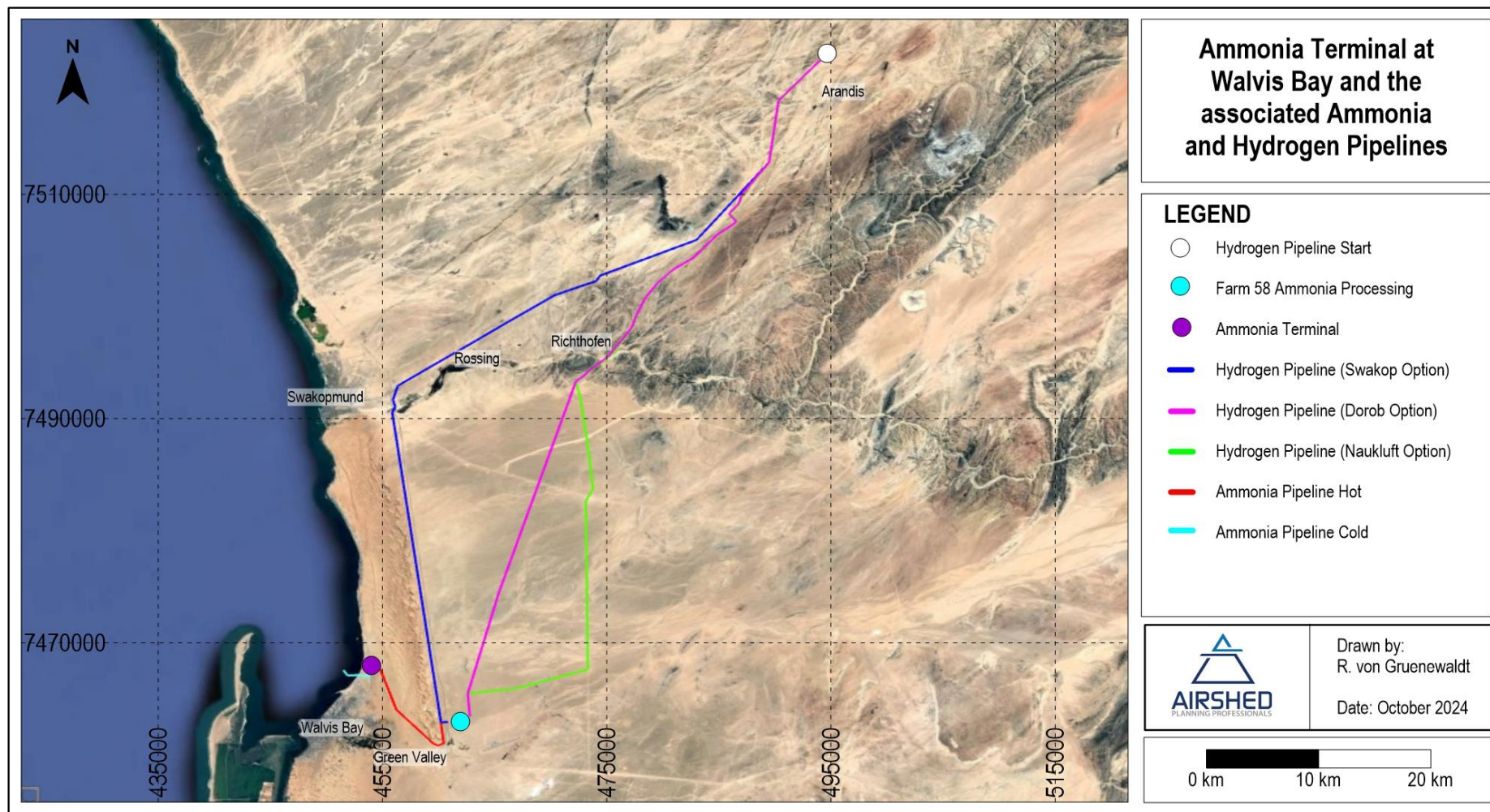


Figure 1-1: The proposed ammonia plant, ammonia terminal, and ammonia and hydrogen pipelines

1.3 Specialist Details

1.3.1 Specialist Details

Airshed is an independent consulting firm with no interest in the project other than to fulfil the contract between the client and the consultant for delivery of specialised services as stipulated in the terms of reference.

1.3.2 Competency Profile of Specialist

Reneé von Gruenewaldt is a Registered Professional Natural Scientist (Registration Number 400304/07) with the South African Council for Natural Scientific Professions (SACNASP) and a member of the National Association for Clean Air (NACA).

Following the completion of her bachelor's degree in atmospheric sciences in 2000 and honours degree (with distinction) with specialisation in Environmental Analysis and Management in 2001 at the University of Pretoria, her experience in air pollution started when she joined Environmental Management Services (now Airshed Planning Professionals) in 2002. Reneé von Gruenewaldt later completed her master's degree (with distinction) in Meteorology at the University of Pretoria in 2009.

Reneé von Gruenewaldt became a partner of Airshed Planning Professionals in September 2006. Airshed Planning Professionals is a technical and scientific consultancy providing scientific, engineering, strategic impact assessments, management services and policy support to assist clients in addressing a wide variety of air pollution and environmental noise related projects.

She has experience on the various components of environmental noise assessments from 2015 to present. Her project experience range over various countries in Africa, providing her with an inclusive knowledge base of international legislation and requirements pertaining to noise impacts.

A comprehensive curriculum vitae of Reneé von Gruenewaldt is provided in Appendix A. Declaration of independence is provided in Appendix B.

1.4 Background to Environmental Noise and the Assessment Thereof

Before more details regarding the approach and methodology adopted in the assessment is given, the reader is provided with some background, definitions and conventions used in the measurement, calculation and assessment of environmental noise.

Noise is generally defined as unwanted sound transmitted through a compressible medium such as air. Sound in turn, is defined as any pressure variation that the ear can detect. Human response to noise is complex and highly variable as it is subjective rather than objective.

A direct application of linear scales (in pascal (Pa)) to the measurement and calculation of sound pressure leads to large and unwieldy numbers. And, as the ear responds logarithmically rather than linearly to stimuli, it is more practical to express acoustic parameters as a logarithmic ratio of the measured value to a reference value. This logarithmic ratio is called a decibel or dB. The advantage of using dB can be clearly seen in Figure 1-2. Here, the linear scale with its large numbers is converted into a manageable scale from 0 dB at the threshold of hearing (20 micro-pascals (μPa)) to 130 dB at the threshold of pain (~100 Pa) (Brüel & Kjær Sound & Vibration Measurement A/S, 2000).

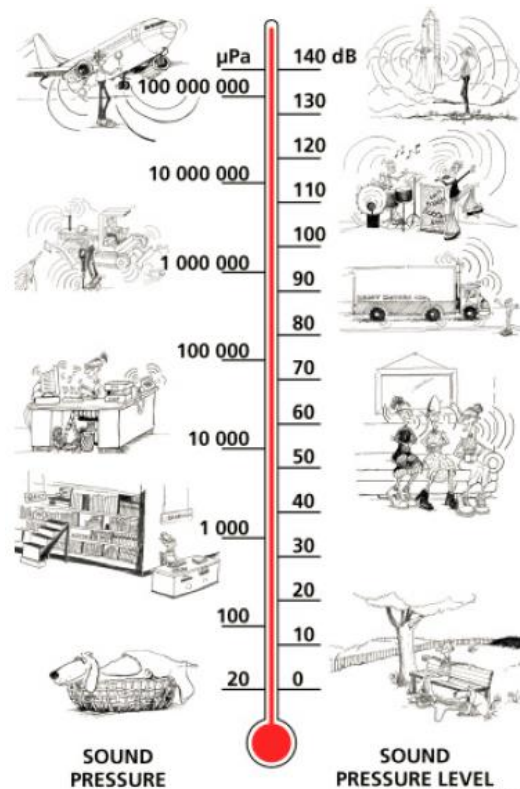


Figure 1-2: The decibel scale and typical noise levels (Brüel & Kjær Sound & Vibration Measurement A/S, 2000)

As explained, noise is reported in dB. “dB” is the descriptor that is used to indicate 10 times a logarithmic ratio of quantities that have the same units, in this case sound pressure. The relationship between sound pressure and sound pressure level is illustrated in this equation.

$$L_p = 20 \cdot \log_{10} \left(\frac{p}{p_{ref}} \right)$$

Where:

L_p is the sound pressure level in dB;

p is the actual sound pressure in Pa; and

p_{ref} is the reference sound pressure (p_{ref} in air is 20 μPa).

1.4.1 Perception of Sound

Sound has already been defined as any pressure variation that can be detected by the human ear. The number of pressure variations per second is referred to as the frequency of sound and is measured in hertz (Hz). The hearing frequency of a young, healthy person ranges between 20 Hz and 20 000 Hz.

In terms of L_p , audible sound ranges from the threshold of hearing at 0 dB to the pain threshold of 130 dB and above. Even though an increase in sound pressure level of 6 dB represents a doubling in sound pressure, an increase of 8 to 10 dB is required before the sound subjectively appears to be significantly louder. Similarly, the smallest perceptible change is about 1 dB (Brüel & Kjær Sound & Vibration Measurement A/S, 2000).

1.4.2 Frequency Weighting

Since human hearing is not equally sensitive to all frequencies, a 'filter' has been developed to simulate human hearing. The 'A-weighting' filter simulates the human hearing characteristic, which is less sensitive to sounds at low frequencies than at high frequencies (Figure 1-3). "dBA" is the descriptor that is used to indicate 10 times a logarithmic ratio of quantities, that have the same units (in this case sound pressure) that has been A-weighted.

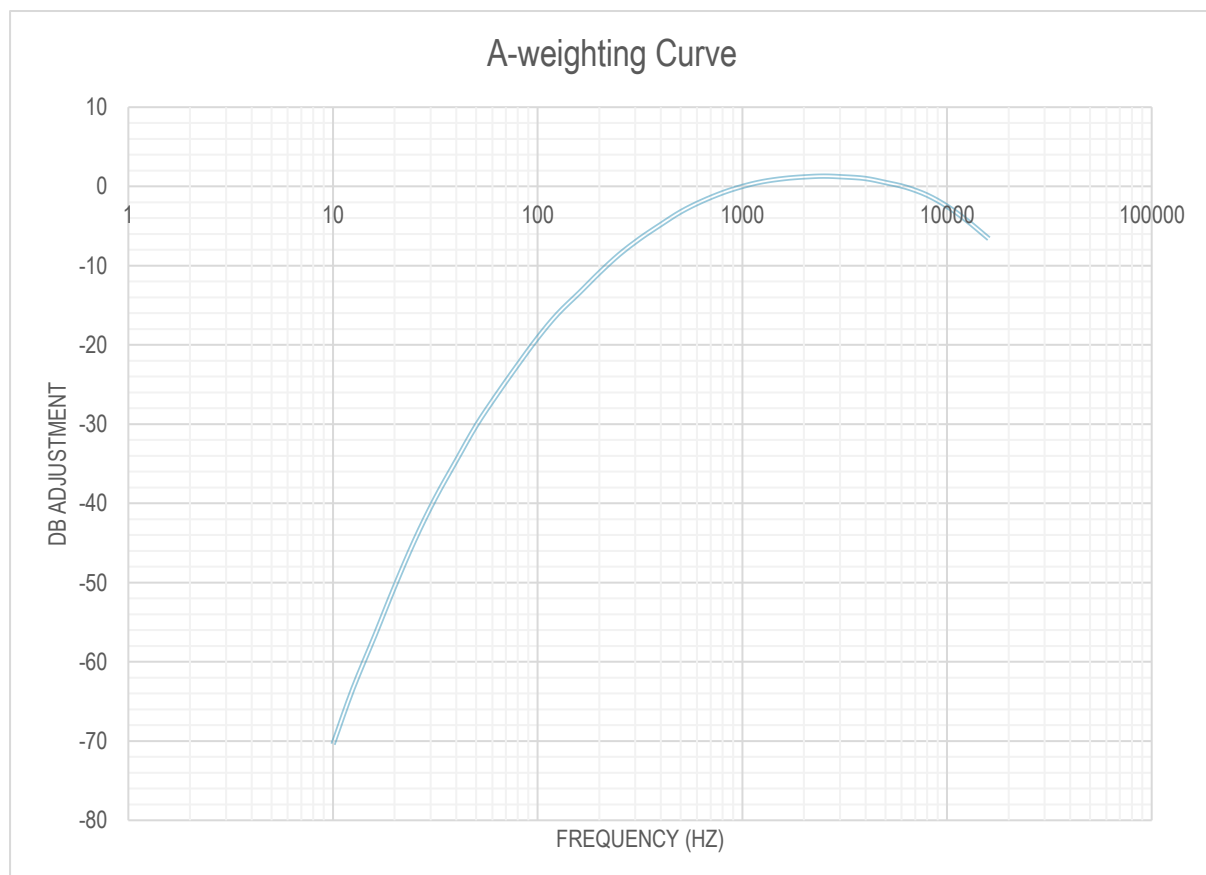


Figure 1-3: A-weighting curve

1.4.3 Adding Sound Pressure Levels

Since sound pressure levels are logarithmic values, the sound pressure levels as a result of two or more sources cannot just simply be added together. To obtain the combined sound pressure level of a combination of sources such as those at an industrial plant, individual sound pressure levels must be converted to their linear values and added using:

$$L_{p_combined} = 10 \cdot \log \left(10^{\frac{L_{p1}}{10}} + 10^{\frac{L_{p2}}{10}} + 10^{\frac{L_{p3}}{10}} + \dots 10^{\frac{L_{pi}}{10}} \right)$$

This implies that if the difference between the sound pressure levels of two sources is nil the combined sound pressure level is 3 dB more than the sound pressure level of one source alone. Similarly, if the difference between the sound pressure levels of two sources is more than 10 dB, the contribution of the quietest source can be disregarded (Brüel & Kjær Sound & Vibration Measurement A/S, 2000).

1.4.4 Environmental Noise Propagation

Many factors affect the propagation of noise from source to receiver. The most important of these are:

- The type of source and its sound power (L_w);
- The distance between the source and the receiver;
- Atmospheric conditions (wind speed and direction, temperature and temperature gradient, humidity etc.);
- Obstacles such as barriers or buildings between the source and receiver;
- Ground absorption; and
- Reflections.

To arrive at a representative result from either measurement or calculation, all these factors must be taken into account (Brüel & Kjær Sound & Vibration Measurement A/S, 2000).

1.4.5 Environmental Noise Indices

In assessing environmental noise either by measurement or calculation, reference is made to the following indices:

- $L_{Aeq}(T)$ – The A-weighted equivalent sound pressure level, where T indicates the time over which the noise is averaged (calculated or measured).
- $L_{Aeq}(T)$ – The impulse corrected A-weighted equivalent sound pressure level, where T indicates the time over which the noise is averaged (calculated or measured). In the South African Bureau of Standards' (SABS) South African National Standard (SANS) 10103 of 2008 for '*The measurement and rating of environmental noise with respect to annoyance and to speech communication*' prescribes the sampling of $L_{Aeq}(T)$.
- L_{A90} – The A-weighted 90% statistical noise level, i.e., the noise level that is exceeded during 90% of the measurement period. It is a very useful descriptor which provides an indication of what the L_{Aeq} could

have been in the absence of noisy single events and is considered representative of background noise levels.

- L_{AFmax} – The maximum A-weighted noise level measured with the fast time weighting. It's the highest level of noise that occurred during a sampling period.
- L_{AFmin} – The minimum A-weighted noise level measured with the fast time weighting. It's the lowest level of noise that occurred during a sampling period.

1.5 Approach and Methodology

The assessment included a study of the legal requirements pertaining to environmental noise impacts, a study of the physical environment of the area surrounding the project and the analyses of existing noise levels in the area. The impact assessment focused on the estimation of L_W 's (noise 'emissions') and L_P 's (noise impacts) associated with the construction phase. The findings of the assessment components informed recommendations of management measures, including mitigation and monitoring. Individual aspects of the noise impact assessment methodology are discussed in more detail below.

1.5.1 Information Review

The following information was supplied for inclusion in the study:

- Layout maps;
- Process description for project operations; and,
- List of equipment and related power ratings for project operations.

1.5.2 Review of Assessment Criteria

In the absence of local guidelines and standards, this study refers to noise level guidelines published by the International Finance Corporation (IFC) in their '*General Environmental, Health, and Safety (EHS) Guidelines*' (IFC, 2007).

In addition to the above reference is also made to very useful indicators of likely community response to an intruding industrial noise as set out by the South African Bureau of Standards' (SABS) South African National Standard (SANS) 10103 of 2008 (SANS 10103, 2008).

1.5.3 Noise Propagation Simulations

The propagation of noise from the project was simulated with the DataKustic CadnaA software. Use was made of the International Organisation for Standardization's (ISO) 9613 module for outdoor noise propagation from industrial noise sources.

ISO 9613 specifies an engineering method for calculating the attenuation of sound during propagation outdoors in order to predict the levels of environmental noise at a distance from a variety of sources. The method predicts the equivalent continuous A-weighted sound pressure level under meteorological conditions favourable to propagation

from sources of known sound emission. These conditions are for downwind propagation or, equivalently, propagation under a well-developed moderate ground-based temperature inversion, such as commonly occurs at night.

The method also predicts an average A-weighted sound pressure level. The average A-weighted sound pressure level encompasses levels for a wide variety of meteorological conditions. The method specified in ISO 9613 consists specifically of octave-band algorithms (with nominal midband frequencies from 63 Hz to 8 kHz) for calculating the attenuation of sound which originates from a point sound source, or an assembly of point sources. The source (or sources) may be moving or stationary. Specific terms are provided in the algorithms for the following physical effects, geometrical divergence, atmospheric absorption, ground surface effects, reflection and obstacles. A basic representation of the model is given in the equation below:

$$L_P = L_W - \sum [K_1, K_2, K_3, K_4, K_5, K_6]$$

Where;

L_P is the sound pressure level at the receiver;

L_W is the sound power level of the source;

K₁ is the correction for geometrical divergence;

K₂ is the correction for atmospheric absorption;

K₃ is the correction for the effect of ground surface;

K₄ is the correction for reflection from surfaces; and

K₅ is the correction for screening by obstacles.

This method is applicable in practice to a great variety of noise sources and environments. It is applicable, directly or indirectly, to most situations concerning road or rail traffic, industrial noise sources, construction activities, and many other ground-based noise sources.

To apply the method of ISO 9613, several parameters need to be known with respect to the geometry of the source and of the environment, the ground surface characteristics, and the source strength in terms of octave-band sound power levels for directions relevant to the propagation.

If the dimensions of a noise source are small compared with the distance to the listener, it is called a point source. All sources of noise were quantified as point sources or areas/lines represented by point sources. The sound energy from a point source spreads out spherically, so that the sound pressure level is the same for all points at the same distance from the source and decreases by 6 dB per doubling of distance. This holds true until ground and air attenuation noticeably affect the level. The impact of an intruding industrial noise on the environment will therefore rarely extend over more than 5 km from the source and is therefore always considered "local" in extent.

The propagation of noise was calculated over an area of 5 km east-west by 5 km north-south. The area was divided into a grid matrix with a 20 m resolution. The model was set to calculate L_P's (L_{Aeq}) at each grid and discrete receptor point at a height of 1.5 m above ground level.

1.5.4 Study of the Receiving Environment

NSRs generally include private residences, community buildings such as schools, hospitals and any publicly accessible areas outside an industrial facility's property. Residential areas included in the assessment as NSRs were identified from available maps and satellite imagery.

1.5.5 Noise Survey

The extent of noise impacts as a result of an intruding noise depends largely on existing noise levels in an area. Higher ambient noise levels will result in less noticeable noise impacts and a smaller impact area. The opposite also holds true. Increases in noise will be more noticeable in areas with low ambient noise levels. The data from a baseline noise survey conducted by ECC in July 2024 was used.

1.5.6 Source Inventory

To determine the change in noise impacts associated with the project, a source inventory had to be developed. A list of equipment was provided and used to compile the source inventory. L_w 's for these were calculated using predictive equations for industrial machinery as per the Handbook of Acoustics, Chapter 69, by Bruce and Moritz (1998).

Noise source L_w 's for the project generator was obtained from a database for similar operations. Values from the database are based on source measurements carried out in accordance with the procedures specified in SANS 10103.

1.5.7 Presentation of Results

Results are presented in isopleth form. An isopleth is a line on a map connecting points at which a given variable (in this case sound pressure, L_p) has a specified constant value. This is analogous to contour lines on a map showing terrain elevation. In the assessment of environmental noise, isopleths present lines of constant noise level as a function of distance.

Simulated noise levels were assessed according to guidelines published in by the IFC.

1.5.8 Recommendations of Management and Mitigation

The findings of the noise specialist study informed the recommendation of suitable noise management and mitigation measures.

1.6 Management of Uncertainties

The following limitations and assumptions should be noted:

- The mitigating effect of buildings, and infrastructure acting as acoustic barriers were not taken into account providing a conservative assessment of the noise impacts off-site.
- The quantification of sources of noise was limited to the operational phase of the project. Construction and closure and decommissioning phase activities are expected to be lower than during the operational phase. Noise impacts will cease post-closure.
- Project operations were assumed to be 24 hours per day.
- The project emergency processes were assumed for an hour.
- Project commissioning operations were assumed for a 24-hour period.
- Although other existing sources of noise within the area were identified during the survey, such sources were not quantified but were taken into account during the baseline sampling.
- The environmental noise assessment focuses on the evaluation of impacts for humans.
- The scope of work did not include a vibration assessment.

2 Legal Requirements and Noise Level Guidelines

The IFC best practice guidelines were adopted in the absence of Namibian legislation.

2.1 International Finance Corporation Guidelines on Environmental Noise

The IFC General Environmental Health and Safety Guidelines on noise address impacts of noise beyond the property boundary of the facility under consideration and provides noise level guidelines.

The IFC states that noise impacts **should not exceed the levels presented in Table 2-1, or** result in a maximum **increase above background levels of 3 dBA** at the nearest receptor location off-site (IFC, 2007). For a person with average hearing acuity an increase of less than 3 dBA in the general ambient noise level is not detectable. $\Delta = 3$ dBA is, therefore, a useful significance indicator for a noise impact.

It is further important to note that the IFC noise level guidelines for residential, institutional and educational receptors correspond with the SANS 10103 guidelines for urban districts.

Table 2-1: IFC noise level guidelines

Area	One Hour L_{Aeq} (dBA) 07:00 to 22:00	One Hour L_{Aeq} (dBA) 22:00 to 07:00
Industrial receptors	70	70
Residential, institutional and educational receptors	55	45

2.2 SANS 10103 Guidance on Estimating Community Response

SANS 10103 (2008) provides a useful guideline for estimating community response to an increase in the general ambient noise level caused by intruding noise. If Δ is the increase in noise level, the following criteria are of relevance:

- $\Delta \leq 0$ dB: There will be no community reaction;
- $0 \text{ dB} < \Delta \leq 10 \text{ dB}$: There will be 'little' reaction with 'sporadic complaints';
- $5 \text{ dB} < \Delta \leq 15 \text{ dB}$: There will be a 'medium' reaction with 'widespread complaints'. $\Delta = 10$ dB is subjectively perceived as a doubling in the loudness of the noise;
- $10 \text{ dB} < \Delta \leq 20 \text{ dB}$: There will be a 'strong' reaction with 'threats of community action'; and,
- $15 \text{ dB} < \Delta$: There will be a 'very strong' reaction with 'vigorous community action'.

The categories of community response overlap because the response of a community does not occur as a stepwise function, but rather as a gradual change.

3 Description of the Receiving Environment

This chapter provides details of the receiving acoustic environment which is described in terms of:

- Local NSRs;
- The local environmental noise propagation and attenuation potential; and
- Current noise levels and the existing acoustic climate.

3.1 Noise Sensitive Receptors

NSRs generally include places of residence and areas where members of the public may be affected by noise generated by proposed activities.

Potential noise sensitive receptors within the study area (Figure 3-1) include the residential area of Walvis Bay.

3.2 Environmental Noise Propagation and Attenuation Potential

3.2.1 Atmospheric Absorption and Meteorology

Atmospheric absorption and meteorological conditions have already been mentioned with regards to their role in the propagation of noise from a source to receiver (Section 1.4.4). The main meteorological parameters affecting the propagation of noise include wind speed, wind direction and temperature. These, along with other parameters such as relative humidity, air pressure, solar radiation and cloud cover affect the stability of the atmosphere and the ability of the atmosphere to absorb sound energy.

Wind speed increases with altitude. This results in the 'bending' of the path of sound to 'focus' it on the downwind side and creating a 'shadow' on the upwind side of the source. Depending on the wind speed, the downwind level may increase by a few dB but the upwind level can drop by more than 20 dB (Brüel & Kjær Sound & Vibration Measurement A/S, 2000). It should be noted that at wind speeds of more than 5 m/s, ambient noise levels are mostly dominated by wind generated noise.

Data from the calculated WRF¹ data for the period 2021 to 2023 was used for the assessment (Figure 3-2). The modelled data set indicates wind flow primarily from the south-southwest and the southwest during the day and night. On average, noise impacts are expected to be slightly more notable to the north-northeast and northeast.

Temperature gradients in the atmosphere create effects that are uniform in all directions from a source. On a sunny day with no wind, temperature decreases with altitude and creates a 'shadowing' effect for sounds. On a clear night, temperatures may increase with altitude thereby 'focusing' sound on the ground surface. Noise impacts are therefore generally more notable during the night (Figure 3-3).

¹ The Weather Research and Forecasting (WRF) Model is a state-of-the-art mesoscale numerical weather prediction system designed for both atmospheric research and operational forecasting applications.

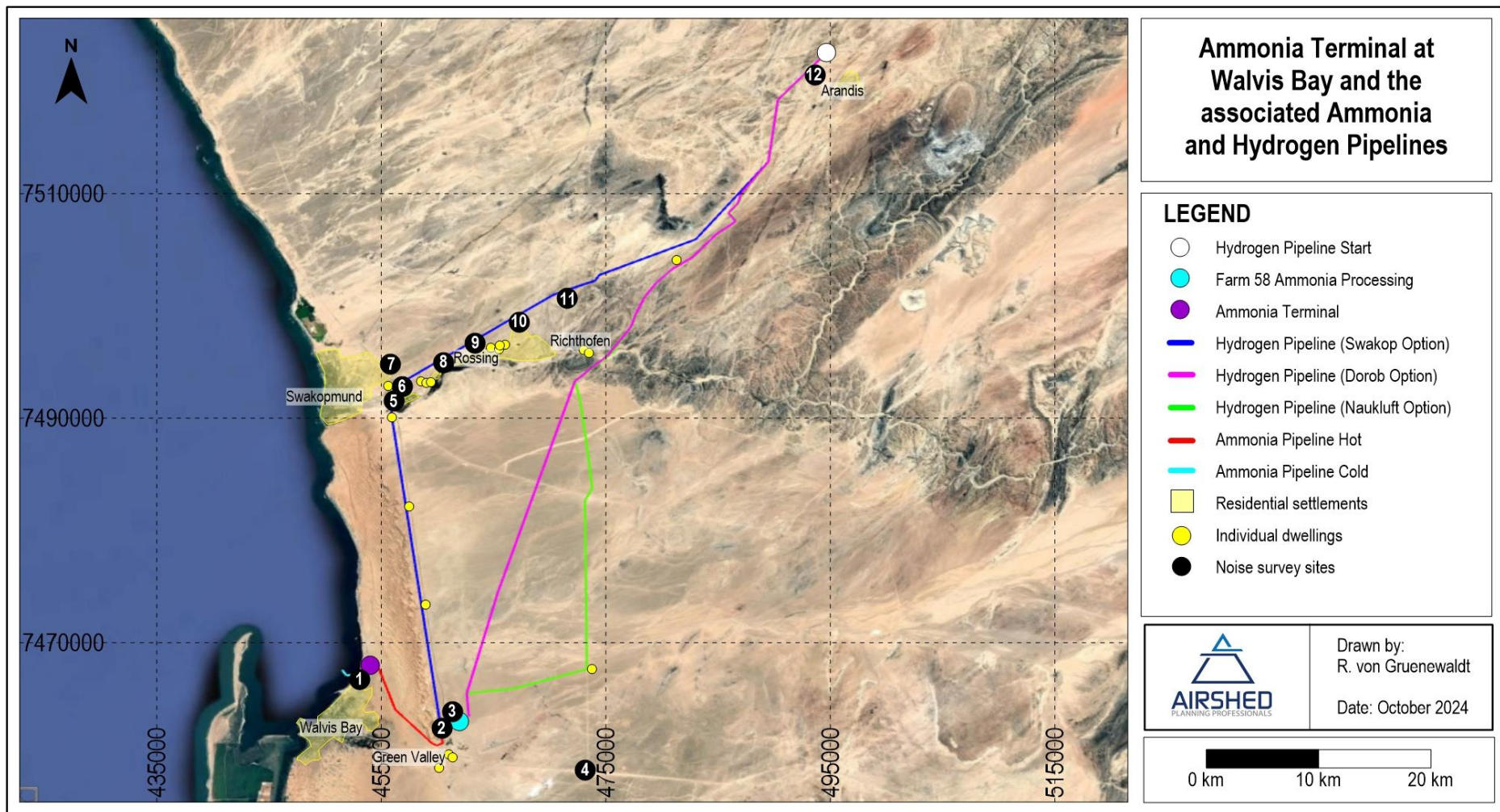


Figure 3-1: Sensitive receptors within the study area and baseline noise survey sites

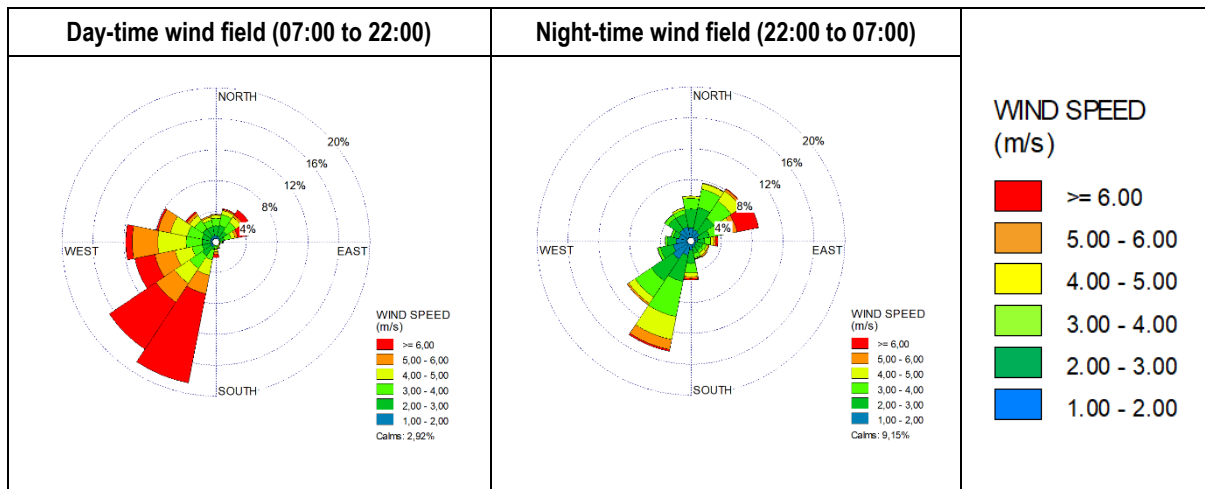


Figure 3-2: Wind rose for Walvis Bay (as obtained from WRF data) for the period 2021 to 2023

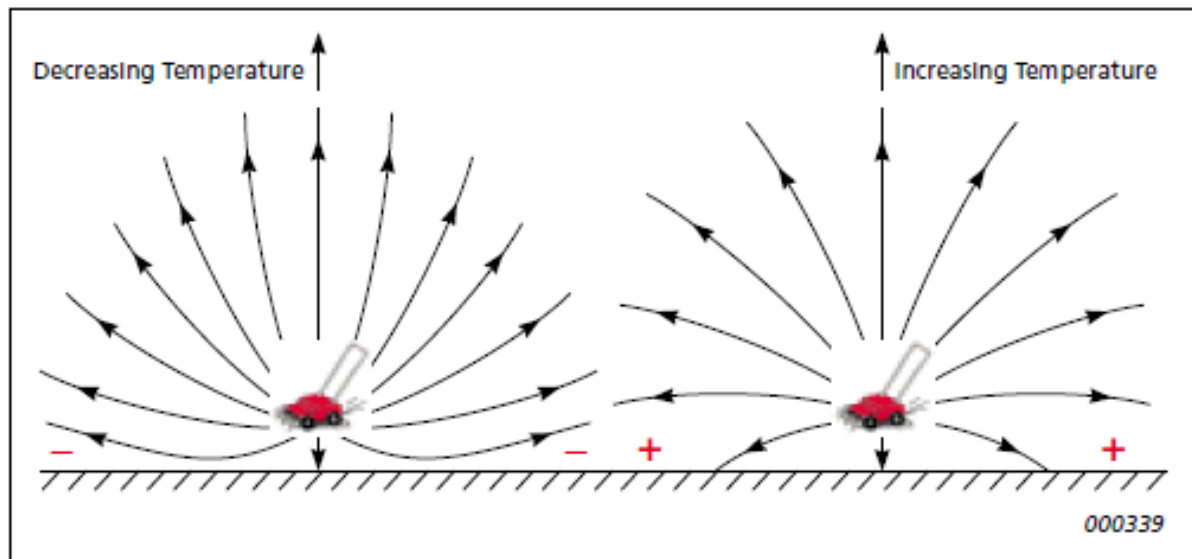


Figure 3-3: Bending the path of sound during typical day time conditions (image provided on the left) and night-time conditions (image provided on the right)

3.2.2 Terrain, Ground Absorption and Reflection

Noise reduction caused by a barrier (i.e., natural terrain, installed acoustic barrier, building) feature depends on two factors namely the path difference of a sound wave as it travels over the barrier compared with direct transmission to the receiver and the frequency content of the noise (Brüel & Kjær Sound & Vibration Measurement A/S, 2000). The topography² for the study area is provided in Figure 3-4.

Sound reflected by the ground interferes with the directly propagated sound. The effect of the ground is different for acoustically hard (e.g., concrete or water), soft (e.g., grass, trees or vegetation) and mixed surfaces. Ground attenuation is often calculated in frequency bands to take into account the frequency content of the noise source

² SRTM1 from the United States Geological Survey at <https://earthexplorer.usgs.gov>

and the type of ground between the source and the receiver (Brüel & Kjær Sound & Vibration Measurement A/S, 2000). Based on observations, ground cover was found to be acoustically mixed.

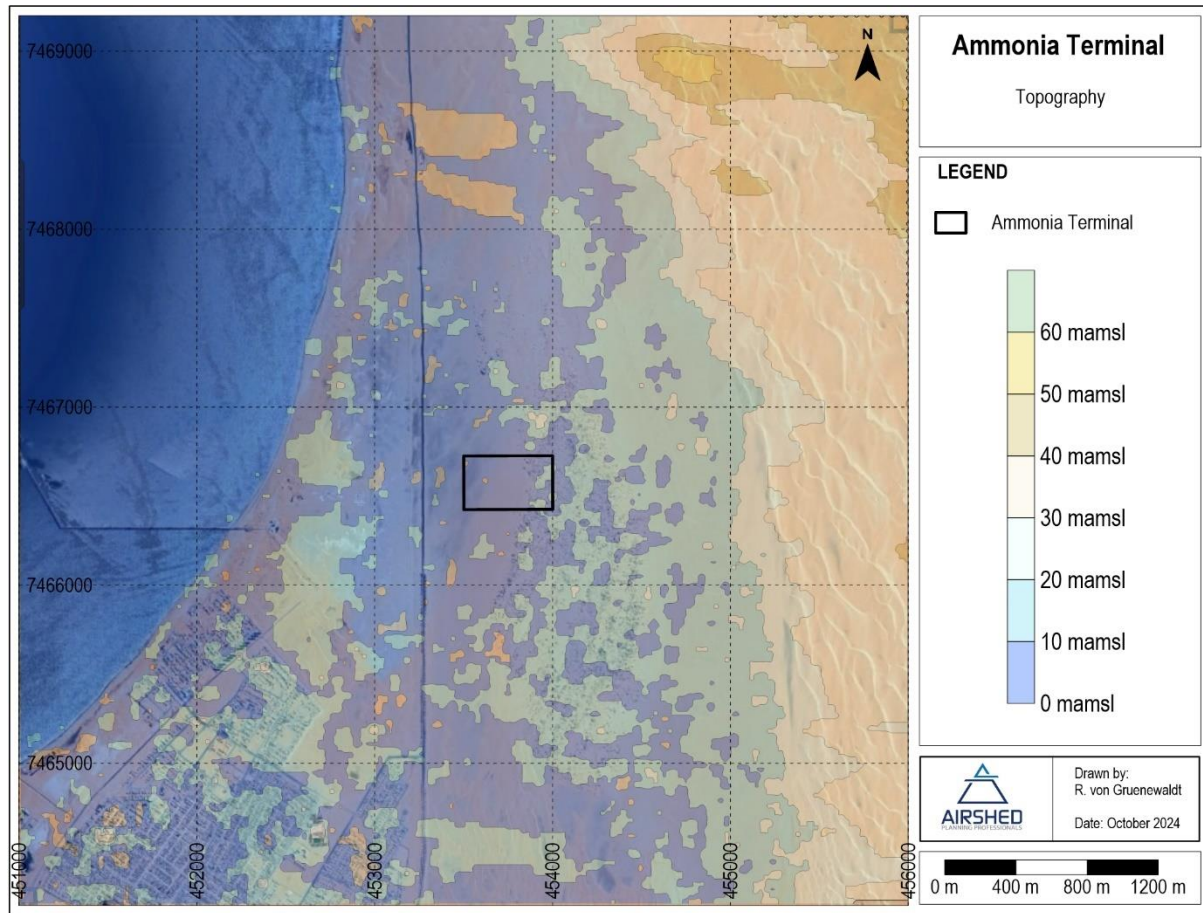


Figure 3-4: Topography for the study area

3.3 Noise Survey and Results

Survey sites were selected after careful consideration of future activities, accessibility, potential noise sensitive receptors, and safety restrictions. A total of 12 survey sites were selected. The location of the noise survey sites is provided in Figure 3-1. Photographs of the sites are included in Appendix C. For detailed time-series, frequency spectra and statistical results, the reader is referred to Appendix D.

Survey results for the campaign undertaken on the 23 to 26 July 2024 are summarised in Table 3-1 and for comparison purposes, visually presented in Figure 3-3 (day-time results) and Figure 3-4 (night-time results).

The survey site in proximity to the project was Site 1 (near Walvis Bay). The noise levels at Site 1 were within the IFC noise guidelines for day- and night-time conditions.

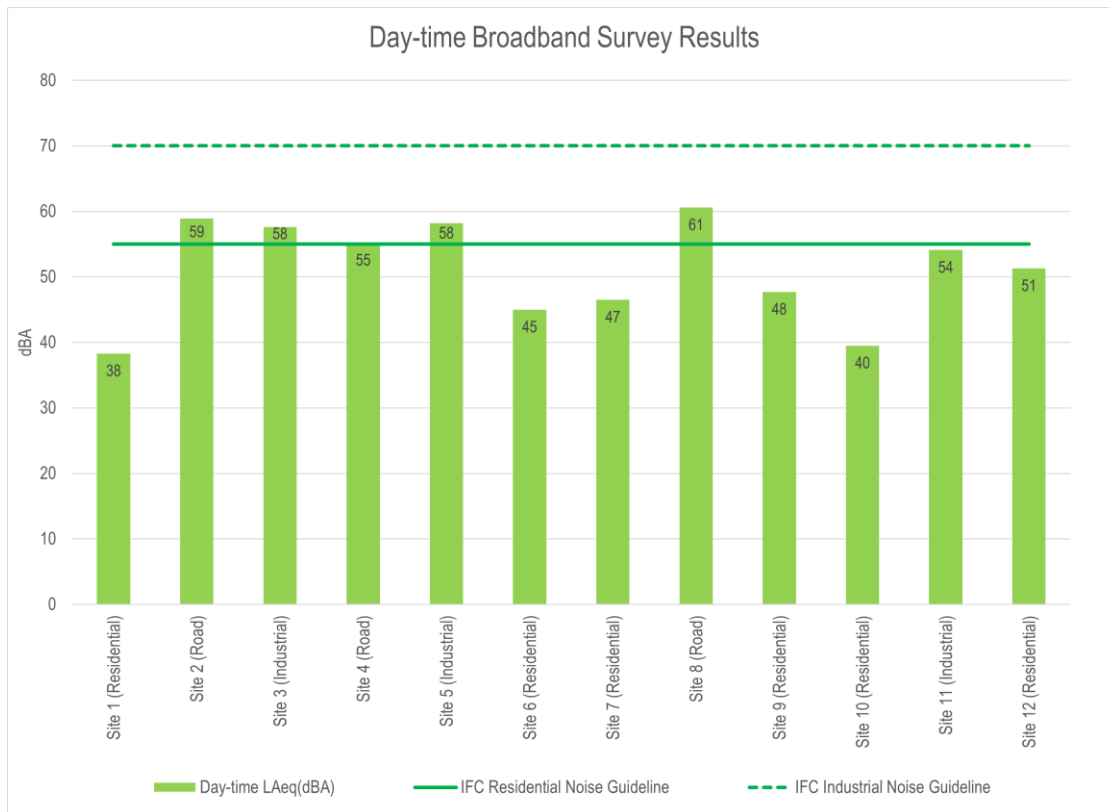


Figure 3-5: Day-time broadband survey results

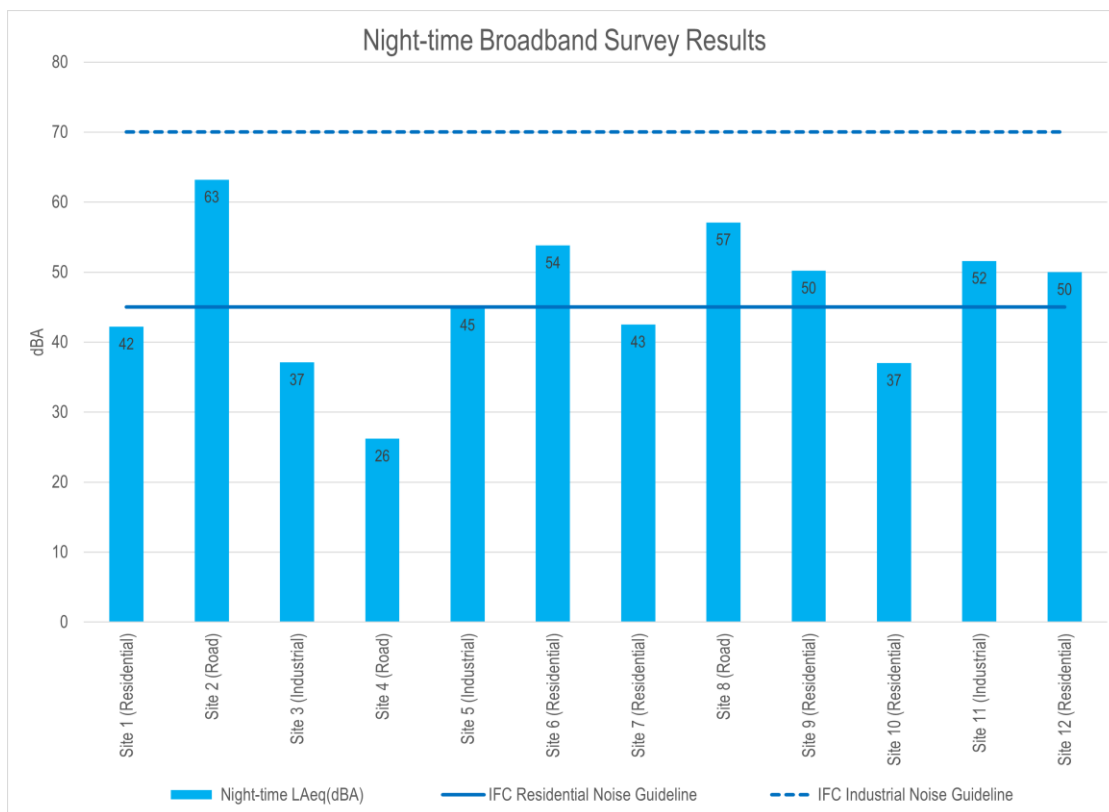


Figure 3-6: Night-time broadband survey results

Table 3-1: Summary of noise measurements conducted in 2024

Sampling point	Visual and acoustic observations	General weather conditions	Time of day	Start date and time	Duration	L _{AFmax} (dBA)	L _{AFmin} (dBA)	L _{Aeq} (dBA) ^(a)	L _{Aeq} (dBA)	L _{A90} (dBA)	IFC Noise Level Guidelines (dBA)
Site 1 (Residential)	Site is just north of Walvis Bay and ~30 m from New Western Avenue Road. Noise sources include dogs, community activities, vehicles, goats and birds.	Winds of 1.1 m/s (N); 11°C; 86% humidity; no cloud cover	Day	2024/07/25 09:59	00:20:26	61.5	29.9	38.3	63.3	33.0	55
		Winds of 1.1 m/s (S); 13°C; 86% humidity; no cloud cover	Night	2024/07/25 22:00	00:20:02	62.9	35.7	42.2	42.7	37.4	45
Site 2 (Road)	Site is ~50 m from the road (D1984). Noise sources include vehicles, construction vehicles, quad bikes, insects and birds.	Winds of 1.6m/s (SW); 15°C; 71% humidity; 40% cloud cover	Day	2024/07/25 11:48	00:20:12	72.1	34.6	58.9	51.9	38.3	N/A
		Winds of 1.6m/s (S); 11°C; 88% humidity; no cloud cover	Night	2024/07/25 23:40	00:20:01	87.0	25.3	63.2	36.9	28.1	N/A
Site 3 (Industrial)	Site is west of construction site. Noise sources include construction vehicles, electrical generators, and workers.	Winds of 2.5 m/s (SW); 17°C; 63% humidity; no cloud cover	Day	2024/07/25 13:11	00:20:01	80.6	47.6	57.6	52.5	50.3	70
		Winds of 1.9 m/s (S); 10°C; 90% humidity; no cloud cover	Night	2024/07/26 00:30	00:20:01	51.0	23.2	37.1	37.4	27.6	70
Site 4 (Road)	Site is ~20 m from unpaved road. Noise sources include vehicles, aircraft, insects and birds.	Winds of 5.5m/s (SW); 18°C; 64% humidity; no cloud cover	Day	2024/07/25 15:20	00:20:01	75.9	26.0	55.2	41.9	33.1	N/A
		Winds of 1.4 m/s (SE); 9°C; 91% humidity; no cloud cover	Night	2024/07/26 01:36	00:20:44	59.0	19.4	26.2	45.2	20.9	N/A
Site 5 (Industrial)	Site is ~30 m from road (C28) and ~200 m from construction site. Noise sources include construction activities, vehicles, birds and insects (night).	Winds of 1.4 m/s (NE); 11°C; 88% humidity; 90% cloud cover	Day	2024/07/24 09:27	00:20:44	73.1	30.2	58.2	59.7	35.9	70
		Winds of 1.7 m/s (NE); 9°C; 94% humidity; no cloud cover	Night	2024/07/25 02:37	00:20:03	69.3	25.8	44.9	46.8	29.5	70
Site 6 (Residential)	Residential area(E), surfaces (desert/sandy soil), Noise sources include community activities, air traffic, vehicles passing, dogs and birds chirping.	Winds of 1.3m/s (SW); 16°C; 68% humidity; 10% cloud cover	Day	2024/07/24 11:33	00:20:07	60.3	32.5	45.0	41.3	35.8	55
		Winds of 1.6m/s (NE); 10°C; 93% humidity; no cloud cover	Night	2024/07/25 01:40	00:20:04	78.8	43.5	53.8	65.2	46.0	45
Site 7 (Residential)	Site is located to the east of a residential area. Noise sources include community activities, aircraft, and vehicles.	Winds of 0.8 m/s (NNE); 12°C; 80% humidity; 70% cloud cover	Day	2024/07/24 10:25	00:20:09	62.8	29.5	46.5	44.6	32.7	55
		Winds of 1.6 m/s (NE); 9°C; 94% humidity; no cloud cover	Night	2024/07/25 03:27	00:20:01	64.2	28.1	42.5	41.0	33.2	45
Site 8 (Road)	Site is located ~25 m from B2 road. Noise sources include vehicles.	Winds of 2.5m/s (SW); 17°C; 61% humidity; 10% cloud cover	Day	2024/07/24 12:40	00:20:03	73.5	32.8	60.6	59.2	41.1	N/A

Sampling point	Visual and acoustic observations	General weather conditions	Time of day	Start date and time	Duration	L _{AFmax} (dBA)	L _{AFmin} (dBA)	L _{Aeq} (dBA) ^(a)	L _{Aeq} (dBA)	L _{A90} (dBA)	IFC Noise Level Guidelines (dBA)
		Winds of 1.1 m/s (E); 8°C; 94% humidity; no cloud cover	Night	2024/07/24 02:47	00:20:02	80.5	20.4	57.1	34.5	22.9	N/A
Site 9 (Residential)	Site is located near residential area. Noise sources include birds, insects (night), community activities, dogs, and vehicles.	Winds of 3.1 m/s (SW); 18°C; 57% humidity; 10% cloud cover	Day	2024/07/24 13:36	00:20:01	58.8	32.4	47.7	45.9	36.0	55
		Winds of 1.3 m/s (SE); 8°C; 95% humidity; no cloud cover	Night	2024/07/24 01:10	00:20:32	66.9	23.8	50.2	36.4	26.4	45
Site 10 (Residential)	Site is located near residential area. Noise sources include birds, community activities, dogs, and vehicles.	Winds of 1.2 m/s (SW); 19°C; 53% humidity; no cloud cover	Day	2024/07/24 14:25	00:20:01	48.8	31.1	39.5	43.8	33.6	55
		Winds of 1.3 m/s (E); 8°C; 93% humidity; no cloud cover	Night	2024/07/24 01:57	00:20:03	52.2	19.8	37.0	39.9	22.2	45
Site 11 (Industrial)	Site is located ~300 m south of NamWater terminal plant. Noise sources include birds and vehicles.	Winds of 3.3 m/s (SW); 19°C; 54% humidity; 10% cloud cover	Day	2024/07/24 15:29	00:20:02	71.2	49.9	54.1	53.3	51.3	70
		Winds of 1.4 m/s (ENE); 10°C; 89% humidity; no cloud cover	Night	2024/07/25 00:35	00:20:07	60.5	47.8	51.6	52.4	49.4	70
Site 12 (Residential)	Site is located ~3 km northwest from Arandis town. Noise sources include dogs, insects, vehicles and community activities.	No wind; 20°C; 56% humidity; 10% cloud cover	Day	2024/07/26 10:49	00:20:38	73.4	31.8	51.3	41.7	33.7	55
		Winds of 2.2 m/s (E); 12°C; 67% humidity; 12% cloud cover	Night	2024/07/23 22:06	00:20:38	69.2	31.4	50.0	47.9	35.3	45

(a) Exceedances of the IFC noise guideline is provided in bold.

N/A: Not applicable

4 Impact Assessment

The noise source inventory, noise propagation modelling and results for the project are discussed in the following section.

4.1 Process Description

4.1.1 Continuous Process

For normal operations the Scrubber and Nitrogen (N₂) and Instrument Air (IA) generation units are assumed to be venting continuously to atmosphere.

4.1.2 Intermittent / Emergency Process

Emergency emissions are just expected during an emergency scenario, and they are supposed to be active for a relatively short period of time. If an emergency is detected in the terminal, the system is designed to trip and flare the operating loads to protect it against undesired events.

Most of the emergency vapor releases either from equipment or along the ammonia transfer lines are routed to the tank outlet vapour line (i.e. connected to the ref. system feed line), recondensed and sent back to the main tank. Except for the relief of the main pressure safety valves (PSVs) on the tank, which are directed to the flare. In case the reference system trips, since there is no possibility of recondensing, the vapours are routed to the flare as well, rather than being treated in the scrubber unit due to the lower treatment capacity than the expected emergency relief.

4.1.2.1 Flare (Tank PSVs Maximum Release)

The worst-case scenario of flaring would be due to a sudden change in the ambient pressure. This affects the relative operating pressure difference between the tank and the environment. A sudden drop in ambient pressure can shift the main storage tank pressure dangerously close to the maximum designed overpressure with the environment. To rapidly relief this pressure, the tank is equipped with a series of 4 PSVs ("T" orifice) with a total rated capacity of 29.1 tph. This amount is such that neither the reference system nor the scrubber is able to cope with, and thus this stream is directed toward the flare for combustion, assisted with propane.

4.1.2.2 Flare (Scrubber Not Available)

In case the scrubber is not operating or is under maintenance, the purge with same flowrate (of 1000 kg/h) and composition is sent to the flare.

4.1.3 Start-up, Commissioning and Decommissioning

During start-up, commissioning and decommissioning it is expected that the flare unit will be operating continuously. The expected maximum flowrate during commissioning is about 2000 kg/h.

4.2 Noise Sources and Sound Power Levels

The complete source inventory for the project is included in Section 4.1. Octave band frequency spectra L_W 's are included in Table 4-2.

The reader is reminded of the non-linearity in the addition of L_W 's. If the difference between the sound power levels of two sources is nil the combined sound power level is 3 dB more than the sound pressure level of one source alone. Similarly, if the difference between the sound power levels of two sources is more than 10 dB, the contribution of the quietest source can be disregarded (Brüel & Kjær Sound & Vibration Measurement A/S, 2000).

Table 4-1: Equipment list for the project

Item	Equipment Description	Qty	Type	Required capacity	Unit
1	Tank Area				
1.1	Storage tank	1	Full containment	40 000	tonne
1.2	Transfer pumps	3	Centrifugal pump, submerged	465	kW
1.3	Cooldown pump	1	Centrifugal pump, submerged	40	kW
2	Transport Area				
2.1	MLA Drain Vessel	1	Horizontal vessel	18	m ³
2.2	Marine Loading Arms	2	Marine un/loading arm with no vapour return	800/ 2660 unloading/ loading	m ³ /hr
3	Refrigeration Area				
3.1	Refrigeration compressor LP Stage	3	Twin screw (oil flooded)	2 240	kg/hr
3.2	Refrigeration compressor HP Stage	3	Twin screw (oil flooded)	3 670	kg/hr
3.3	Refrigeration ammonia pumps	2	Centrifugal pump	70	m ³ /hr
3.4	Refrigeration K.O. drum	1	Horizontal vessel	20	m ³
3.5	Refrigeration economizer	1	Horizontal vessel	40	m ³
3.6	Refrigeration liquid receiver	1	Horizontal vessel	20	m ³
3.7	Condensers	3	Air cooler	1 317	kW
3.8	Vacuum breaker heater	1	Air heater		
4	Scrubber Unit (4400)				
4.1	Aqueous ammonia scrubber	1	Horizontal vessel with vertical tower	5	m ³
4.2	Aqueous ammonia pumps	2	Centrifugal pump	5	m ³
4.3	Aqueous ammonia scrubber heat exchanger	2	Plate heat exchanger	20	kW
5	Flare Unit (4300)				
5.1	Flare K.O. vessel	1	Horizontal vessel	7.5	m ³

Item	Equipment Description	Qty	Type	Required capacity	Unit
5.2	Flare stack	1	Self-supporting	29 100	kg/hr
5.3	Flare tip	1	Open pipe fuel assisted	29 100	kg/hr
5.4	Fuel storage tank to flare	1	Horizontal vessel	67.7	m ³
6	Nitrogen Unit (PU-0200)				
6.1	I.A. Buffer vessel	1	Vertical vessel	3	m ³
6.2	N ₂ Buffer vessel	1	Vertical vessel	10	m ³
6.3	Air Buffer vessel	1	Vertical vessel	3	m ³
6.4	Dryers	2	Chiller	350	m ³ /hr
6.5	Absorption columns	2		69.6	m ³ /hr
6.6	Air compressor	2	Screw compressor	250	Nm ³ /hr
6.7	Intake air filter	1		576	m ³ /hr
6.8	Discharge particle air filter	1		576	m ³ /hr
7	Water Utilities Unit				
7.1	Firewater storage tank	1	Vertical vessel	2 400	m ³
7.2	Drinking water storage tank	1	Vertical vessel	10	m ³
7.3	Jockey pump	1	Centrifugal pump	10	m ³ /hr
7.4	Firewater pump	1	Centrifugal pump	681.3	m ³ /hr
7.5	Jockey pump	1	Centrifugal pump	10	m ³ /hr
7.6	Firewater pump	1	Centrifugal pump	681.3	m ³ /hr
7.7	Potable water pump	2	Centrifugal pump	8	m ³ /hr
7.8	Drinking water pump	1	Centrifugal pump	2	m ³ /hr
7.9	Denim water package	1		4	m ³ /hr
7.9.1	Denim water filtration unit	1	Reverse osmosis	4	m ³ /hr
7.9.2	Denim water pump	2	Centrifugal pump	4	m ³ /hr
7.9.3	Denim water storage vessel	1	Vertical vessel	10	m ³
8	Emergency Diesel Generator (PU-0100)				
8.1	Diesel storage tank	1	Storage tank	26 000	L
8.2	Emergency power generation unit	1	Diesel generator	1	MW
8.3	Diesel pump	2	Centrifugal pump	3	m ³ /hr
9	Sewage System				
9.1	Effluent lift pump	1	Centrifugal pump	40	m ³ /hr
9.2	Rainwater collection vessel	1	Underground pit	200	m ³
9.3	Spill tank	1	Underground pit	50	m ³

Table 4-2: Octave band frequency spectra L_w 's

Equipment	Type	L _w octave band frequency spectra (dB)								L _w (dB)	L _{WA} (dBA)	Source
		63 Hz	125 Hz	250 Hz	500 Hz	1000 Hz	2000 Hz	4000 Hz	8000 Hz			
Refrigeration pumps (x4)	L _w	75.8	76.8	78.8	78.8	81.8	78.8	74.8	68.8	87.0	85.4	L _w Predictions (Bruce & Moritz, 1998)
Condensers (x9)	L _w	100.2	99.2	97.2	97.2	99.2	103.2	102.2	98.2	109.1	108.1	L _w Predictions (Bruce & Moritz, 1998)
NH ₃ compressor (x4)	L _w	95.5	94.5	92.5	92.5	94.5	98.5	97.5	93.5	104.5	103.5	L _w Predictions (Bruce & Moritz, 1998)
Jockey pump (x2)	L _w	71.5	72.5	74.5	74.5	77.5	74.5	70.5	64.5	82.7	81.1	L _w Predictions (Bruce & Moritz, 1998)
Firewater pump (x2)	L _w	75.5	76.5	78.5	78.5	81.5	78.5	74.5	68.5	86.7	85.1	L _w Predictions (Bruce & Moritz, 1998)
Potable water pump (x4)	L _w	71.5	72.5	74.5	74.5	77.5	74.5	70.5	64.5	82.7	81.1	L _w Predictions (Bruce & Moritz, 1998)
Drinking water pump	L _w	71.5	72.5	74.5	74.5	77.5	74.5	70.5	64.5	82.7	81.1	L _w Predictions (Bruce & Moritz, 1998)
Denim water package (x2)	L _w	71.5	72.5	74.5	74.5	77.5	74.5	70.5	64.5	82.7	81.1	L _w Predictions (Bruce & Moritz, 1998)
Emergency power generation unit	L _w	119.2	109.1	108.9	109.2	106.0	100.8	94.0		120.5	110.5	L _w database
Diesel pump (x4)	L _w	71.5	72.5	74.5	74.5	77.5	74.5	70.5	64.5	82.7	81.1	L _w Predictions (Bruce & Moritz, 1998)
Effluent lift pump	L _w	71.5	72.5	74.5	74.5	77.5	74.5	70.5	64.5	82.7	81.1	L _w Predictions (Bruce & Moritz, 1998)

The sound power level for the elevated flare was calculated based on the German recognised Standard – VDI 3272 standard noise levels of flares:

$$L_{wac} = 112(\pm 6) + 17 \log Q$$

Where:

L_{wac} = A-weighted sound power level of the flare (dBA)

Q = flare gas mass flow (t/h)

The height of the flare was provided as 50 m. An exit velocity and exit temperature of 20 m/s and 1 000°C respectively was provided. The flowrates and the calculated sound power levels for the different project operating scenarios is provided in Table 4-3.

Table 4-3: Calculated sound power levels for the flare

Operating Conditions	Flowrate (kg/hr)	A-weighted sound power level of the flare (dBA)
Emergency Process - Tank PSVs max. release	29 100	142.9
Emergency Process - Scrubber not available	1 000	118.0
Continuous Process - Commissioning	2 000	123.1

4.3 Noise Propagation and Simulated Noise Levels

The propagation of noise generated during the operational phase was calculated with CadnaA in accordance with ISO 9613. Meteorological and site-specific acoustic parameters as discussed in Section 3.2 along with source data discussed in 4.1, were applied in the model.

Table 4-3 provides a summary of simulated noise levels for the project at NSRs within the study area. Simulated noise levels due to project only are also presented in the form of isopleth plots (Figure 4-1 and Figure 4-2).

Noise levels due to project operations will result in the following noise impacts at the closest NSR (i.e. Walvis Bay) (Table 4-4):

- Normal project operations:
 - Day-time: no exceedances of the IFC noise guideline for residential areas;
 - Night-time: no exceedances of the IFC noise guideline for residential areas;
- Emergency project activities (where the ammonia release from the main PSVs on the tank are released through the flare for an hour):
 - Day-time: no exceedances of the IFC noise guideline for residential areas;
 - Night-time: noise levels (53.2 dBA) exceed the IFC noise guideline (45 dBA) for residential areas;
- Emergency project activities (scrubber not available and throughput released through the flare for an hour):
 - Day-time: no exceedances of the IFC noise guideline for residential areas;

- Night-time: no exceedances of the IFC noise guideline for residential areas;
- Project commissioning operations:
 - Day-time: no exceedances of the IFC noise guideline for residential areas;
 - Night-time: no exceedances of the IFC noise guideline for residential areas.

For a person with average hearing acuity an increase of less than 3 dBA in the general ambient noise level is not detectable. According to SANS 10103 (2008); the predicted increase in noise levels from the current baseline due to project operations only is expected to result in the following community reaction (Table 4-4):

- Normal project operations: no community reaction;
- Emergency project activities (where the ammonia release from the main PSVs on the tank are released through the flare for an hour): 'medium' community reaction with widespread complaints;
- Emergency project activities (scrubber not available and throughput released through the flare for an hour): no community reaction;
- Project commissioning operations: no community reaction.

Table 4-4: Summary of simulated noise levels (provided as dBA) due to the proposed project activities at the closest NSR (Walvis Bay)

Operating Condition	IFC Noise Guidelines		Project operations (a)		Baseline (b)		Increase Above Baseline (c)	
	Day-time	Night-time	Day	Night	Day	Night	Day	Night
Continuous Process	55	45	23.1	24.7	38.3	42.2	0.1	0.1
Emergency Process - Tank PSVs max. release	55	45	48.7	53.2	38.3	42.2	10.8	11.3
Emergency Process - Scrubber not available	55	45	25.9	29.6	38.3	42.2	0.2	0.2
Continuous Process - Commissioning	55	45	40.4	41.7	38.3	42.2	4.2	2.8

Notes:

- (a) Exceedance of the IFC noise guideline is provided in bold.
- (b) Baseline measurements based on closest or representative sampling sites and reflective of current noise levels in the area.
- (c) Likely community response in accordance with the SANS 10103:

< 3 dBA	< 5 dBA	< 10 dBA	< 15 dBA	< 20 dBA
Change imperceptible	No reaction	'Little' reaction with sporadic complaints	'Medium' reaction with widespread complaints	'Strong' to 'very strong' reaction with threats of community action or vigorous community action.

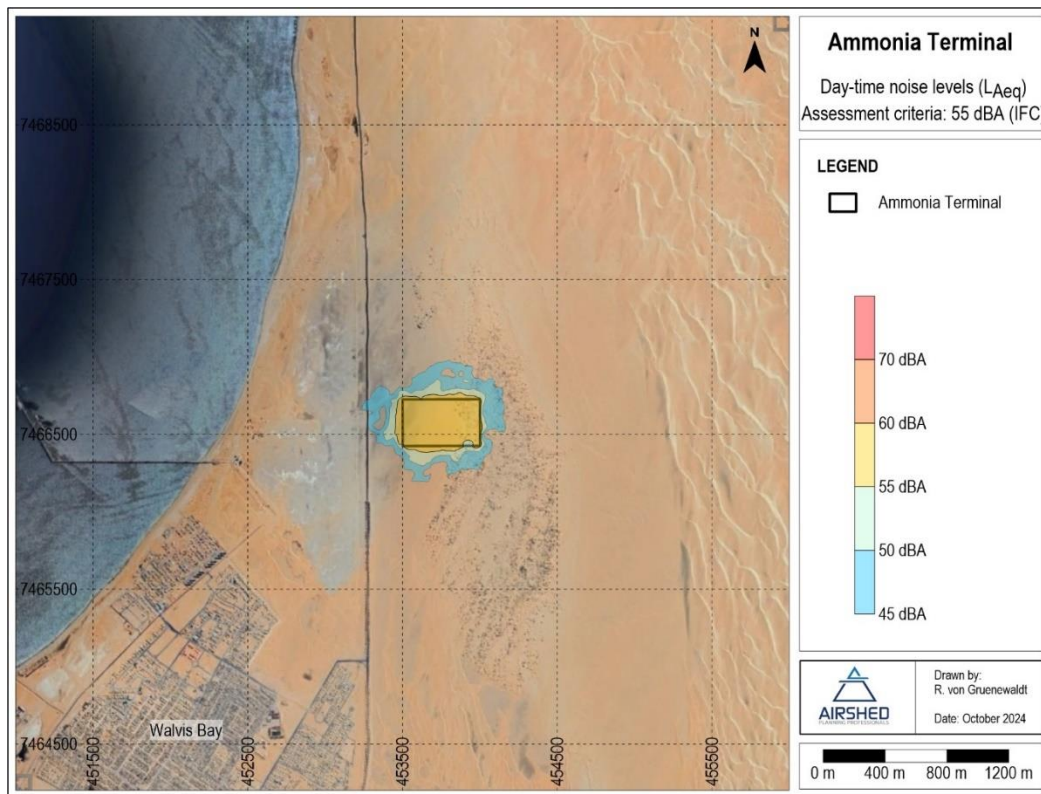


Figure 4-1: Simulated day-time noise levels due to normal project operations only

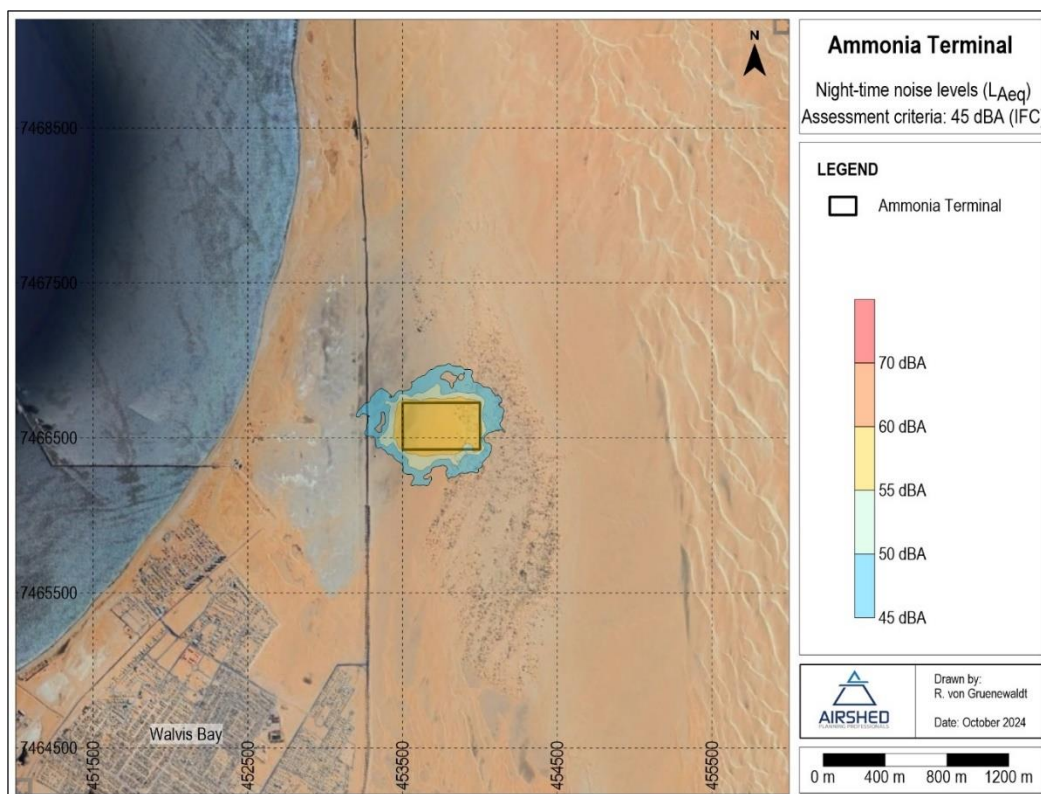


Figure 4-2: Simulated night-time noise levels due to normal project operations only

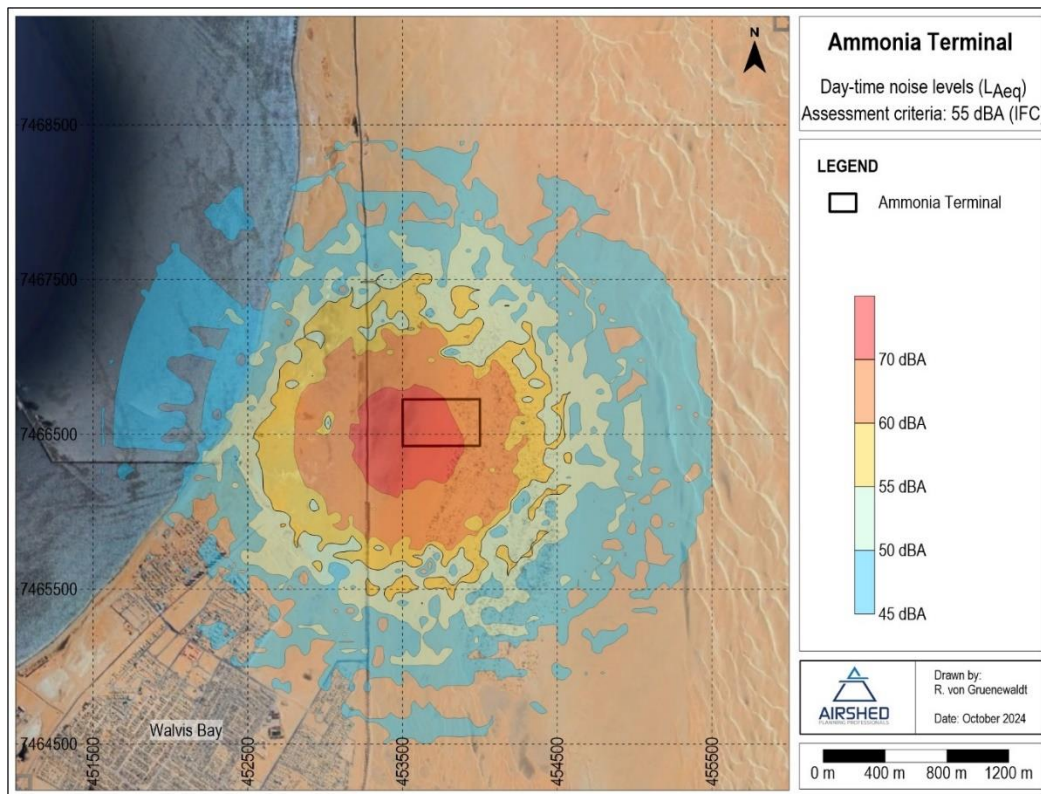


Figure 4-3: Simulated day-time noise levels due to project emergency process (assuming 1 hr tank PSVs maximum release through the flare)

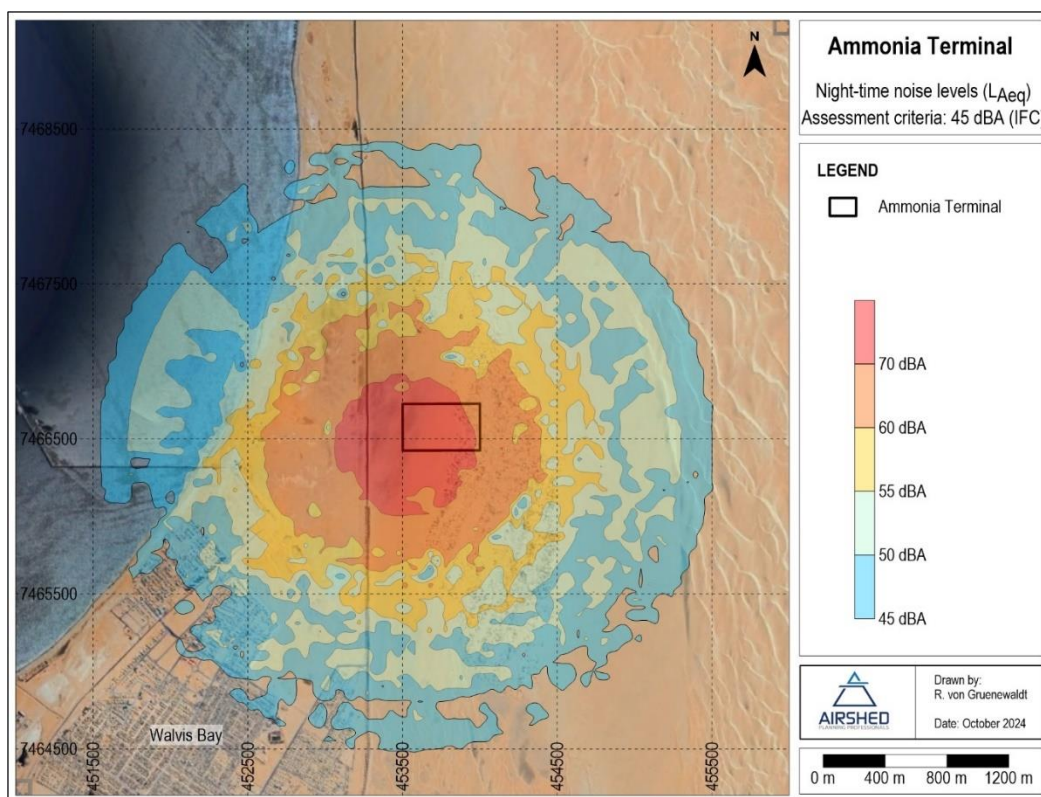


Figure 4-4: Simulated night-time noise levels due to project emergency process (assuming 1 hr tank PSVs maximum release through the flare)

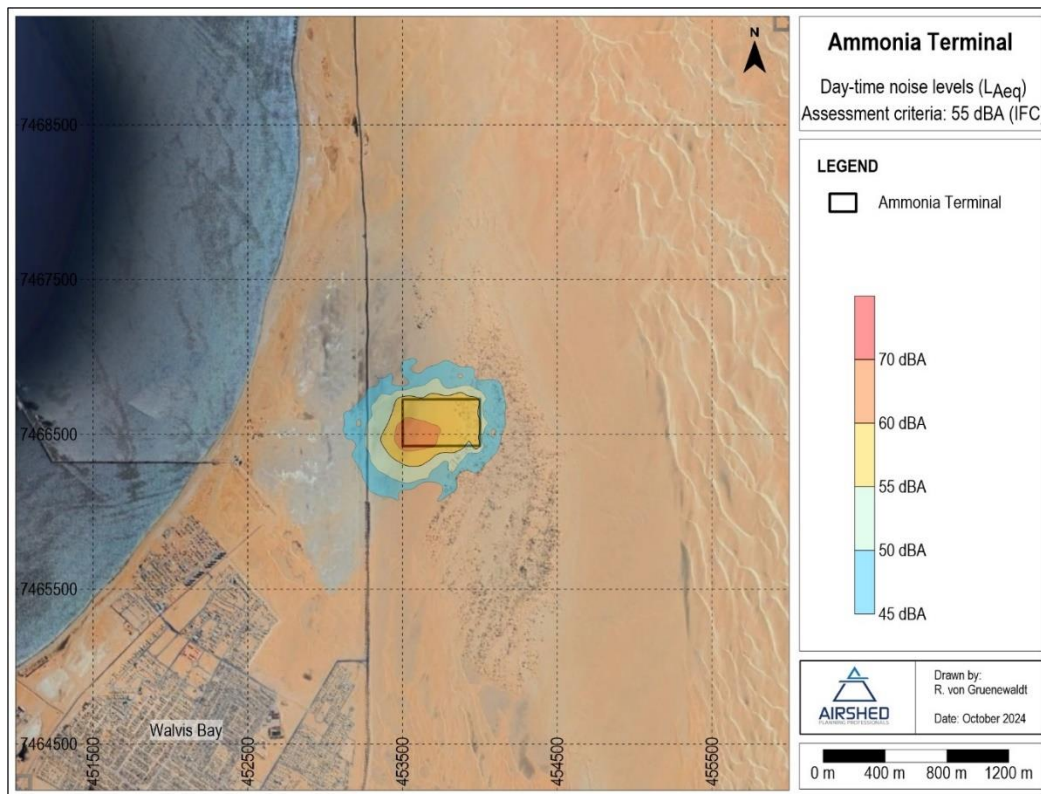


Figure 4-5: Simulated day-time noise levels due to project emergency process (assuming 1 hr Scrubber emission release through the flare)

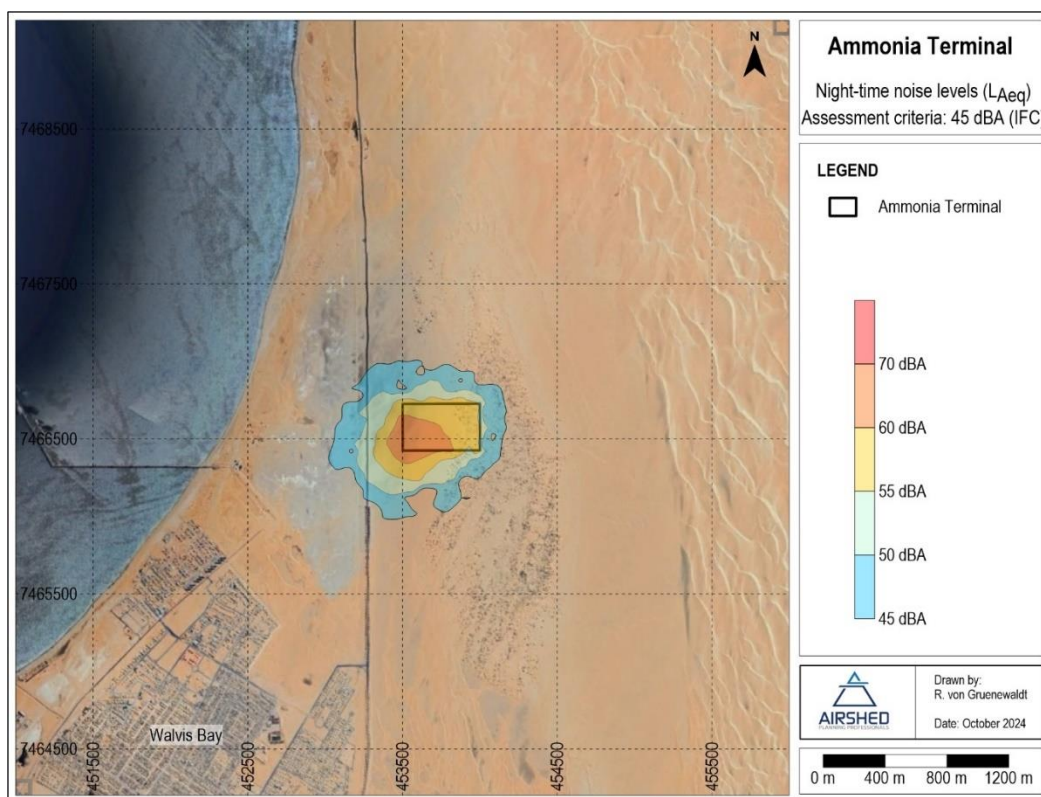


Figure 4-6: Simulated night-time noise levels due to project emergency process (assuming 1 hr Scrubber emission release through the flare)

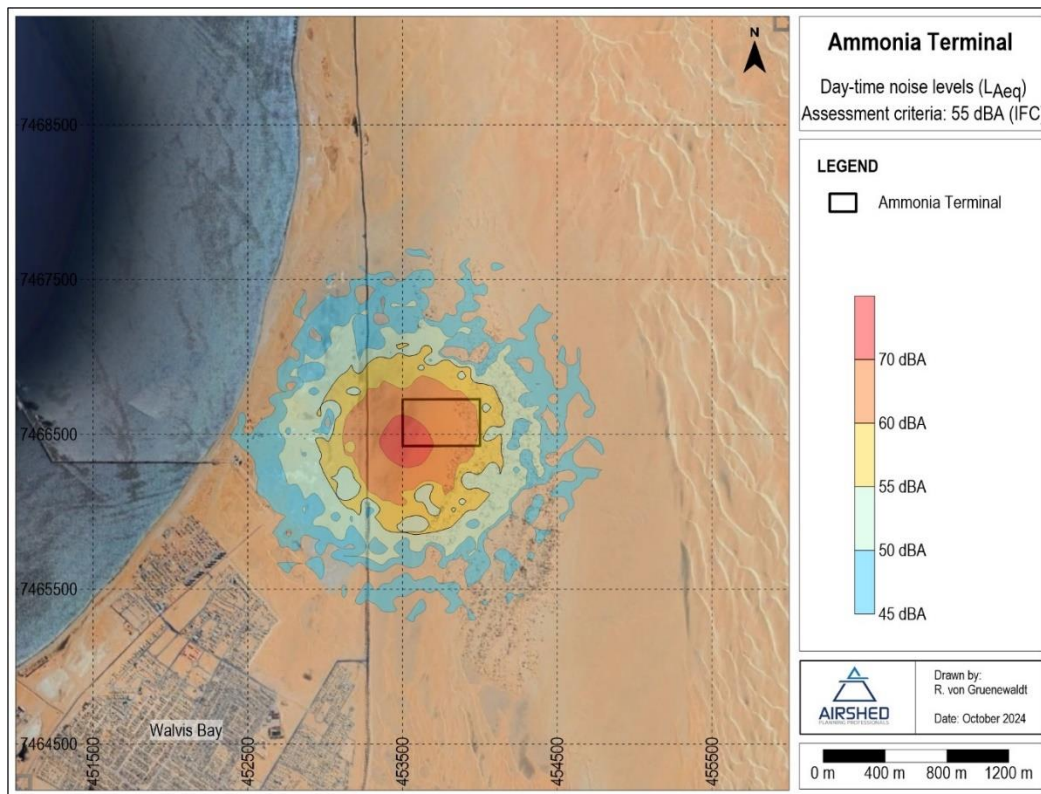


Figure 4-7: Simulated day-time noise levels due to project commissioning operations only

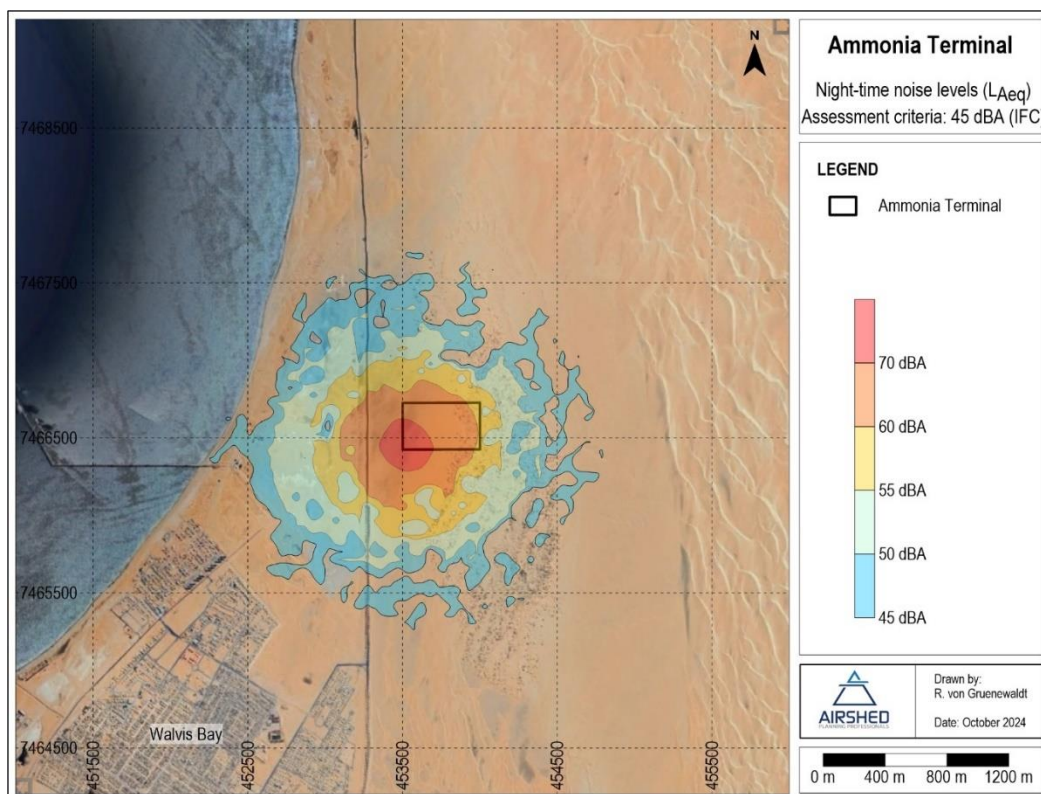


Figure 4-8: Simulated night-time noise levels due to project commissioning operations only

5 Management Measures

In the quantification of noise emissions and simulation of noise levels as a result of the project, it was found that environmental noise evaluation criteria for residential, educational, and institutional receptors will be met for day-time conditions at off-site NSRs for normal operating conditions, project commissioning and emergency conditions if the scrubber is off-line. The potential to exceed IFC noise guidelines at Walvis Bay exists for night-time conditions in the event of a worst-case scenario of flaring due to a sudden change in the ambient pressure. This would result in a maximum release from the tank PSVs through the flare and is active for a relatively short period of time. It should be noted that this is a worst-case scenario and is not a normal operating condition.

The measures discussed in this section are measures typically applicable to industrial sites and are considered good practice by the IFC (2007) and British Standard BSI (2014).

It should be noted that not all mitigation measures are to be implemented, but should the need arise the mitigation measures as discussed in this section can be considered.

5.1 Controlling Noise at the Source

5.1.1 General Good Practice Measures

Good engineering and operational practices will reduce levels of annoyance. For general activities, the following good engineering practice **should** be applied to **construction and closure activities**:

- All diesel-powered equipment and plant vehicles should be kept at a **high level of maintenance**. This should particularly include the regular inspection and, if necessary, replacement of intake and exhaust silencers. Any change in the noise emission characteristics of equipment should serve as trigger for withdrawing it for maintenance.
- In managing noise specifically related to vehicles, efforts **should** be directed at:
 - Minimising individual vehicle engine, transmission, and body noise/vibration. This is achieved through the implementation of an equipment maintenance program.
 - Avoid unnecessary equipment idling at all times.
 - Minimising the need for trucks/equipment to reverse. This will reduce the frequency at which disturbing but necessary reverse warnings will occur. Alternatives to the traditional reverse 'beeper' alarm such as a 'self-adjusting' or 'smart' alarm could be considered. These alarms include a mechanism to detect the local noise level and automatically adjust the output of the alarm is so that it is 5 to 10 dB above the noise level near the moving equipment.
- Unless it is an emergency situation, non-routine noisy activities such as construction, decommissioning, start-up and maintenance, should be limited to day-time hours.
- A noise complaints register must be kept.

5.1.2 Specifications and Equipment Design

Equipment can be reviewed to ensure the quietest available technology is used. Where equipment with lower sound power levels is selected, vendors/contractors should be required to guarantee optimised equipment design noise levels.

5.1.3 Enclosures

As far as is practically possible, sources of significant noise should be enclosed. The extent of enclosure will depend on the nature of the machine and their ventilation requirements. Compressors and pumps are examples of such equipment. Enclosure of the flare can also significantly reduce the noise from this source.

It should be noted that the effectiveness of partial enclosures and screens can be reduced if used incorrectly, e.g. noise should be directed into a partial enclosure and not out of it, there should not be any reflecting surfaces such as parked vehicles opposite the open end of a noise enclosure.

5.1.4 Use and Siting of Equipment and Noise Sources

Recommendations on use and siting of equipment is as follows:

- a) Machines used intermittently should be shut down between work periods or throttled down to a minimum and not left running unnecessarily. This will reduce noise and conserve energy.
- b) Plants or equipment from which noise generated is known to be particularly directional, should be orientated so that the noise is directed away from NSRs.
- c) Acoustic covers of engines should be kept closed when in use or idling.
- d) Doors to pump houses should be kept closed at all times.
- e) Construction materials such as beams should be lowered and not dropped.

5.2 Monitoring

Given the distance of the closest NSRs from the project and that IFC guidelines are not predicted to be exceeded at NSRs due to routine project operations, routine noise monitoring is not recommended.

In the event, however, that noise related complaints are received short term ambient noise measurements should be conducted as part of investigating the complaints. The results of the measurements should be used to inform any follow up interventions. The investigation of complaints should include an investigation into equipment or machinery that likely result or resulted in noise levels annoying to the community. This could be achieved with source noise measurements.

The following procedure should be adopted for all noise surveys:

- Any surveys should be designed and conducted by a **trained specialist**.

- Sampling should be carried out using a **Type 1** Sound Level Meter (SLM) that meets all appropriate International Electro Technical Commission (IEC) standards and is subject to **annual calibration** by an accredited laboratory.
- The **acoustic sensitivity of the SLM should be tested** with a portable acoustic calibrator before and after each sampling session.
- Samples sufficient for statistical analysis should be taken with the use of portable SLM's capable of logging data continuously over the time period. Samples representative of the day- and night-time acoustic environment should be taken.
- The following acoustic indices should be recorded and reported: $L_{Aeq}(T)$, statistical noise level L_{A90} , L_{AFmin} and L_{AFmax} , octave band or 3rd octave band frequency spectra.
- The SLM should be located approximately 1.5 m above the ground and no closer than 3.5 m to any reflecting surface.
- Efforts should be made to ensure that measurements are not affected by the residual noise and extraneous influences, e.g., wind, electrical interference and any other non-acoustic interference, and that the instrument is operated under the conditions specified by the manufacturer. It is good practice to avoid conducting measurements when the wind speed is more than 5 m/s, while it is raining or when the ground is wet.
- A detailed log and record should be kept. Records should include site details, weather conditions during sampling and observations made regarding the acoustic environment of each site.

6 Conclusion

Based on the findings of the assessment for normal project operations and provided the recommended general “good practice” management and mitigation measures are in place, it is the specialist opinion that the ammonia terminal may be authorised from an environmental noise perspective.

7 References

Bruce, R. D. & Moritz, C. T., 1998. Sound Power Level Predictions for Industrial Machinery. In: M. J. Crocker, ed. *Handbook of Acoustics*. Hoboken: John Wiley & Sons, Inc, pp. 863-872.

Brüel & Kjær Sound & Vibration Measurement A/S, 2000. *www.bksv.com*. [Online] Available at: <http://www.bksv.com> [Accessed 14 October 2011].

IFC, 2007. *General Environmental, Health and Safety Guidelines*, s.l.: s.n.

SANS 10103, 2008. *The Measurement and Rating with Environmental Noise with Respect to Annoyance and to Speech Communication*, Pretoria: Standards South Africa.

Appendix A – Specialist Curriculum Vitae

CURRICULUM VITAE

RENEÉ VON GRUENEWALDT

FULL CURRICULUM VITAE

Name of Firm	Airshed Planning Professionals (Pty) Ltd
Name of Staff	Reneé von Gruenewaldt (<i>nee</i> Thomas)
Profession	Air Quality and Environmental Noise Scientist
Position	Principal consultant
Date of Birth	13 May 1978
Years with Firm	Since January 2002
Nationalities	South African

MEMBERSHIP OF PROFESSIONAL SOCIETIES

- Registered Professional Natural Scientist (Registration Number 400304/07) with the South African Council for Natural Scientific Professions (SACNASP)
- Member of the National Association for Clean Air (NACA)

KEY QUALIFICATIONS

Reneé von Gruenewaldt (Air Quality Scientist): Reneé joined Airshed Planning Professionals (Pty) Ltd (previously known as Environmental Management Services cc) in 2002. She has, as a Specialist, attained over twenty (20) years of experience in the Earth and Natural Sciences sector in the field of Air Quality and nine (9) years of experience in the field of environmental noise assessments. As an environmental practitioner, she has provided solutions to both large-scale and smaller projects within the mining, minerals, and process industries.

She has developed technical and specialist skills in various air quality modelling packages including the AMS/EPA Regulatory Models (AERMOD and AERMET), UK Gaussian plume model (ADMS), EPA Regulatory puff-based model (CALPUFF and CALMET), puff-based HAWK model and line-based models, Lagrangian GRAL model. Her experience with air emission models includes Tanks 4.0 (for the quantification of tank emissions), WATER9 (for the quantification of wastewater treatment works) and GasSim (for the quantification of landfill emissions). Noise propagation modelling proficiency includes CONCAWE, South African National Standards (SANS 10210) for calculating and predicting road traffic noise and CadnaA for propagation of industrial, road and rail noise sources.

Having worked on projects throughout Africa (i.e., South Africa, Mozambique, Malawi, Kenya, Angola, Democratic Republic of Congo, Namibia, Madagascar and Egypt for Air Quality Impact Assessments and Mozambique, Namibia, Botswana, Kenya, Ghana, Suriname and Afghanistan for Environmental Noise Impact Assessments) Reneé has developed a broad experience base. She has a good understanding of the laws and regulations associated with ambient air quality and emission limits in South Africa and various other African countries, as well as the World Bank Guidelines, European Community Limits and World Health Organisation.

RELEVANT EXPERIENCE (AIR QUALITY)

Mining and Ore Handling

Reneé has undertaken numerous air quality impact assessments and management plans for coal, platinum, uranium, copper, cobalt, chromium, fluorspar, bauxite, manganese and mineral sands mines. These include: compilation of emissions databases for Landau and New Vaal coal collieries (SA), impact assessments and management plans for numerous mines over Mpumalanga (viz. Schoonoord, Belfast, Goedgedvonden, Mbila, Evander South, Driefontein, Hartogshoop, Belfast, New Largo, Geluk, etc.), Mmamabula Coal Colliery (Botswana), Moatize Coal Colliery (Mozambique), Revuboe Coal Colliery (Mozambique), Toliera Sands Heavy Minerals Mine and Processing (Madagascar), Corridor Sands Heavy Minerals Mine monitoring assessment, El Burullus Heavy Minerals Mine and processing (Egypt), Namakwa Sands Heavy Minerals Mine (SA), Tenke Copper Mine and Processing Plant (DRC), Rössing Uranium (Namibia), Lonmin platinum mines including operations at Marikana, Baobab, Dwaalkop and Doornvlei (SA), Impala Platinum (SA), Pilannesburg Platinum (SA), Aquarius Platinum, Hoogland Platinum Mine (SA), Tamboti PGM Mine (SA), Sari Gunay Gold Mine (Iran), chrome mines in the Steelpoort Valley (SA), Mecklenburg Chrome Mine (SA), Naboom Chrome Mine (SA), Kinsenda Copper Mine (DRC), Kassinga Mine (Angola) and Nokeng Fluorspar Mine (SA), etc.

Mining monitoring reviews have also been undertaken for Optimum Colliery's operations near Hendrina Power Station and Impunzi Coal Colliery with a detailed management plan undertaken for Morupule (Botswana) and Glencor (previously known as Xstrata Coal South Africa).

Air quality assessments have also been undertaken for mechanical appliances including the Durban Coal Terminal and Nacala Port (Mozambique) as well as rail transport assessments including BHP-Billiton Bauxite transport (Suriname), Nacala Rail Corridor (Mozambique and Malawi), Kusile Rail (SA) and WCL Rail (Liberia).

Metal Recovery

Air quality impact assessments have been carried out for Highveld Steel, Scaw Metals, Lonmin's Marikana Smelter operations, Saldanha Steel, Tata Steel, Afro Asia Steel and Exxaro's Manganese Pilot Plant Smelter (Pretoria).

Chemical Industry

Comprehensive air quality impact assessments have been completed for NCP (including Chloorkop Expansion Project, Contaminated soils recovery, C3 Project and the 200T Receiver Project), Revertex Chemicals (Durban), Stoppani Chromium Chemicals, Foskor (Richards Bay), Straits Chemicals (Coega), Tenke Acid Plant (DRC), and Omnia (Sasolburg).

Petrochemical Industry

Numerous air quality impact assessments have been completed for Sasol (including the postponement/exemption application for Synfuels, Infrachem, Natref, MIBK2 Project, Wax Project, GTL Project, re-commissioning of boilers at Sasol Sasolburg and Ekandustria), Engen Emission Inventory Functional Specification (Durban), Sapref refinery (Durban), Sasol (at Elrode) and Island View (in Durban) tanks quantification, Petro SA and Chevron (including the postponement/exemption application).

Pulp and Paper Industry

Air quality studies have been undertaken on the expansion of Mondi Richards Bay, Multi-Boiler Project for Mondi Merebank (Durban), impact assessments for Sappi Stanger, Sappi Enstra (Springs), Sappi Ngodwana (Nelspruit) and Pulp United (Richards Bay).

Power Generation

Air quality impact assessments have been completed for numerous Eskom coal fired power station studies including the ash expansion projects at Kusile, Kendal, Hendrina, Kriel and Arnot; Fabric Filter Plants at Komati, Grootvlei, Tutuka, Lethabo and Kriel Power Stations; the proposed Kusile, Medupi (including the impact assessment for the Flue Gas Desulphurization) and Vaal South Power Stations. Reneé was also involved in the cumulative assessment of the existing and return to service Eskom power stations assessment and the optimization of Eskom's ambient air quality monitoring network over the Highveld.

In addition to Eskom's coal fired power stations, various Eskom nuclear power supply projects have been completed including the air quality assessment of Pebble Bed Modular Reactor and nuclear plants at Duvnefontein, Bantamsklip and Thyspunt.

Apart from Eskom projects, power station assessments have also been completed in Kenya (Rabai Power Station) and Namibia (Paratus Power Plant).

Waste Disposal

Air quality impact assessments, including odour and carcinogenic and non-carcinogenic pollutants were undertaken for the Waste Water Treatment Works in Magaliesburg, proposed Waterval Landfill (near Rustenburg), Tutuka Landfill, Mogale General Waste Landfill (adjacent to the Leipardsvlei Landfill), Cape Winelands District Municipality Landfill, the Tsoeneng Landfill (Lesotho) and the FG Landfill (near the Midstream Estate). Air quality impact assessments have also been completed for the BCL incinerator (Cape Town), the Ergo Rubber Incinerator and the Ecorevert Pyrolysis Plant.

Cement Manufacturing

Impact assessments for ambient air quality have been completed for the Holcim Alternative Fuels Project (which included the assessment of the cement manufacturing plants at Ulco and Dudfield as well as a proposed blending platform in Roodepoort).

Management Plans

Reneé undertook the quantification of the baseline air quality for the first declared Vaal Triangle Airshed Priority Area. This included the establishment of a comprehensive air pollution emissions inventory, atmospheric dispersion modelling, focusing on impact area "hotspots" and quantifying emission reduction strategies. The management plan was published in 2009 (Government Gazette 32263).

Reneé has also been involved in the Provincial Air Quality Management Plan for the Limpopo Province.

RELEVANT EXPERIENCE (GREENHOUSE GAS EMISSION FOOT-PRINTING AND CLIMATE CHANGE IMPACT STATEMENTS)

Mining and Tailings Storage Facilities

Reneé has quantified the direct and indirect (Scope 2 and Scope 3) emissions for numerous mines over the highveld of South Africa and the Democratic Republic of Congo. She has also assessed the climate risks and vulnerabilities of the project and surrounding communities due to increasing ambient temperatures, water scarcity, risk of intense storms.

Gas to Power Plants

Reneé has quantified the direct and indirect (Scope 2 and Scope 3) emissions for gas to power plants proposed for South Africa. She has also assessed the climate risks and vulnerabilities of the project and surrounding communities due to increasing ambient temperatures, water scarcity, risk of intense storms.

RELEVANT EXPERIENCE (NOISE)

Mining

Reneé has undertaken numerous environmental noise assessments for mining operations. These include environmental noise impact assessments including baseline noise surveys for numerous coal, platinum, manganese, tin and zinc mines. Projects include, but are not limited to, Balama (Mozambique), Masama Coal (Botswana), Lodestone (Namibia), Osino (Namibia), Kurmuk (Ethiopia), Gamsberg (SA), Prieska (SA), Kolomela (SA), Heuningkranz (SA), Syferfontein (SA), South 32 (SA), Mamatwan (SA), Alexander (SA) and Marula Platinum Mine (SA), etc.

Power Generation

Environmental noise assessments have been completed for numerous Eskom coal fired power station studies in SA including the Kriel Fabric Filter Plant, Kendal ash facility, Medupi ash facility. Apart from Eskom projects, power plant assessments have also been completed in Botswana (Morupule), Kenya (Or Power geothermal power plants), Suriname (EBS power plant) and SA (Richards Bay combined cycle power plant).

Process Operations

Environmental noise assessments have been undertaken for various process operations including waste disposal facilities (Bon Accord in Gauteng), bottling and drink facilities (Imali and Isanti Project in Gauteng) and Smelter (Gamsberg in Northern Cape).

Transport

An environmental noise assessment was completed for the Obetsebi road expansion and flyover project in Ghana, the Scorpion Zinc Mine transport route in Namibia and the Sisian-Kajaran (North-South Corridor) Road Project in Armenia.

Gas Pipelines

An environmental noise assessment was completed for the Sheberghan gas pipeline in Afghanistan.

Baseline Noise Surveys

Baseline noise surveys have been undertaken for numerous mining and process operation activities (including Raumix quarries, Kolomela and Sibanye Stillwater Platinum Mines (SA)) in support of onsite Environmental Management Programmes.

OTHER EXPERIENCE (2001)

Research for B.Sc Honours degree was part of the "Highveld Boundary Layer Wind" research group and was based on the identification of faulty data from the Majuba Sodar. The project was THRIP funded and was a joint venture with the University of Pretoria, Eskom and Sasol (2001).

EDUCATION

M.Sc Earth Sciences	University of Pretoria, RSA, Cum Laude (2009) Title: <i>An Air Quality Baseline Assessment for the Vaal Airshed in South Africa</i>
B.Sc Hons. Earth Sciences	University of Pretoria, RSA, Cum Laude (2001) Environmental Management and Impact Assessments
B.Sc Earth Sciences	University of Pretoria, RSA, (2000) Atmospheric Sciences: Meteorology

ADDITIONAL COURSES

CALMET/CALPUFF	Presented by the University of Johannesburg, RSA (March 2008)
Air Quality Management	Presented by the University of Johannesburg, RSA (March 2006)

COUNTRIES OF WORK EXPERIENCE

South Africa, Mozambique, Botswana, Ghana, Suriname, Afghanistan, Malawi, Liberia, Kenya, Angola, Democratic Republic of Congo, Ethiopia, Afghanistan, Lesotho, Namibia, Madagascar, Egypt, Suriname and Iran.

EMPLOYMENT RECORD

January 2002 - Present

Airshed Planning Professionals (Pty) Ltd, (previously known as Environmental Management Services cc until March 2003), Principal Air Quality and Environmental Noise Scientist, Midrand, South Africa.

2001

University of Pretoria, Demi for the Geography and Geoinformatics department and a research assistant for the Atmospheric Science department, Pretoria, South Africa.

Department of Environmental Affairs and Tourism, assisted in the editing of the Agenda 21 document for the world summit (July 2001), Pretoria, South Africa.

1999 - 2000

The South African Weather Services, vacation work in the research department, Pretoria, South Africa.

CONFERENCE AND WORKSHOP PRESENTATIONS AND PAPERS

- Understanding the Synoptic Systems that lead to Strong Easterly Wind Conditions and High Particulate Matter Concentrations on The West Coast of Namibia, H Liebenberg-Enslin, R von Gruenewaldt, H Rauntenbach and L Burger. National Association for Clean Air (NACA) conference, October 2017.
- Topographical Effects on Predicted Ground Level Concentrations using AERMOD, R.G. von Gruenewaldt. National Association for Clean Air (NACA) conference, October 2011.
- Emission Factor Performance Assessment for Blasting Operations, R.G. von Gruenewaldt. National Association for Clean Air (NACA) conference, October 2009.
- Vaal Triangle Priority Area Air Quality Management Plan – Baseline Characterisation, R.G. Thomas, H Liebenberg-Enslin, N Walton and M van Nierop. National Association for Clean Air (NACA) conference, October 2007.
- A High-Resolution Diagnostic Wind Field Model for Mesoscale Air Pollution Forecasting, R.G. Thomas, L.W. Burger, and H Rautenbach. National Association for Clean Air (NACA) conference, September 2005.
- Emissions Based Management Tool for Mining Operations, R.G. Thomas and L.W. Burger. National Association for Clean Air (NACA) conference, October 2004.
- An Investigation into the Accuracy of the Majuba Sodar Mixing Layer Heights, R.G. Thomas. Highveld Boundary Layer Wind Conference, November 2002.

LANGUAGES

	Speak	Read	Write
English	Excellent	Excellent	Excellent
Afrikaans	Fair	Fair	Fair

CERTIFICATION

I, the undersigned, certify that to the best of my knowledge and belief, these data correctly describe me, my qualifications, and my experience.



Signature of staff member

29/07/2024

Date (Day / Month / Year)

Full name of staff member:

Renee Georgeinna von Gruenewaldt

Appendix B – Declaration of Independence

DECLARATION OF INDEPENDENCE - PRACTITIONER

Name of Practitioner: Renée von Gruenewaldt

Name of Registration Body: South African Council for Natural Scientific Professions

Professional Registration No.: 400304/07

Declaration of independence and accuracy of information provided:

Environmental Noise Impact Assessment for the Ammonia Terminal, Close to Walvis Bay

I, Renée von Gruenewaldt, declare that I am independent of the applicant. I have the necessary expertise to conduct the assessments required for the report and will perform the work relating the application in an objective manner, even if this results in views and findings that are not favourable to the applicant. I will disclose to the applicant and the air quality officer all material information in my possession that reasonably has or may have the potential of influencing any decision to be taken with respect to the application by the air quality officer. The additional information provided in this atmospheric impact report is, to the best of my knowledge, in all respects factually true and correct. I am aware that the supply of false or misleading information to an air quality officer is a criminal offence in terms of section 51(1)(g) of this Act.

Signed at Pretoria on this 30th of October 2024.



SIGNATURE

Principal Noise Scientist

CAPACITY OF SIGNATORY

Appendix C – Survey Site Photos



Figure C-1: Photographs of environmental noise Site 1



Figure C-2: Photographs of environmental noise Site 2

Facing north



Facing east



Facing south



Facing west



Figure C-3: Photographs of environmental noise Site 3

Facing north



Facing east



Facing south



Facing west



Figure C-4: Photographs of environmental noise Site 4

Facing north



Facing east



Facing south



Facing west



Figure C-5: Photographs of environmental noise Site 5

Facing north



Facing east



Facing south



Facing west



Figure C-6: Photographs of environmental noise Site 6

Facing north



Facing east



Facing south



Facing west



Figure C-7: Photographs of environmental noise Site 7

Facing north



Facing east



Facing south



Facing west



Figure C-8: Photographs of environmental noise Site 8

Facing north



Facing south



Facing east



Facing west



Figure C-9: Photographs of environmental noise Site 9

Facing north



Facing south



Facing east



Facing west



Figure C-10: Photographs of environmental noise Site 10

Facing north



Facing east



Facing south



Facing west



Figure C-11: Photographs of environmental noise Site 11

Facing north



Facing east



Facing south



Facing west



Figure C-12: Photographs of environmental noise Site 12

Appendix D – Time-series, Statistical, and Frequency Spectrum Results

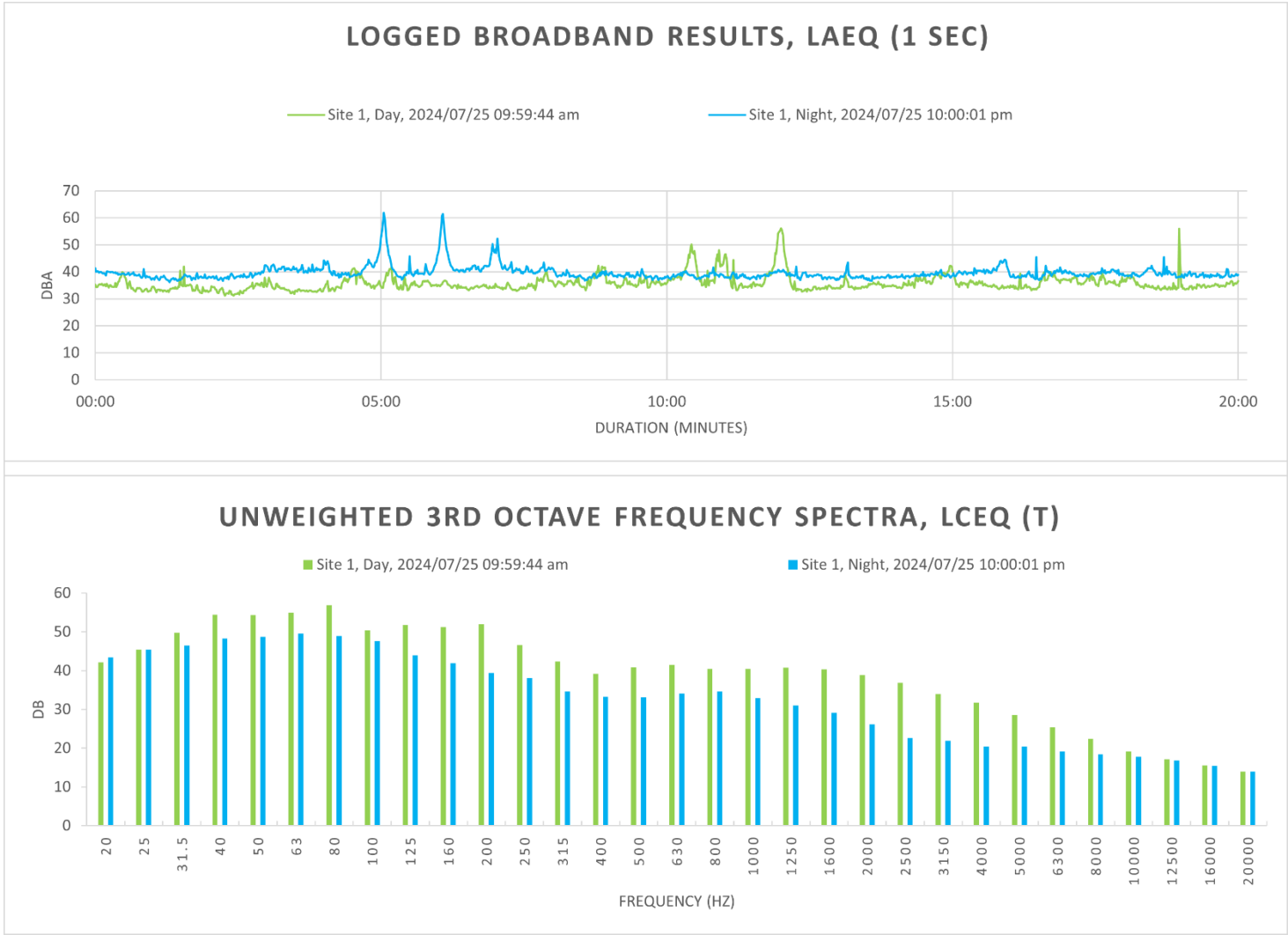


Figure D-1: Detailed day- and night-time survey results for Site 1

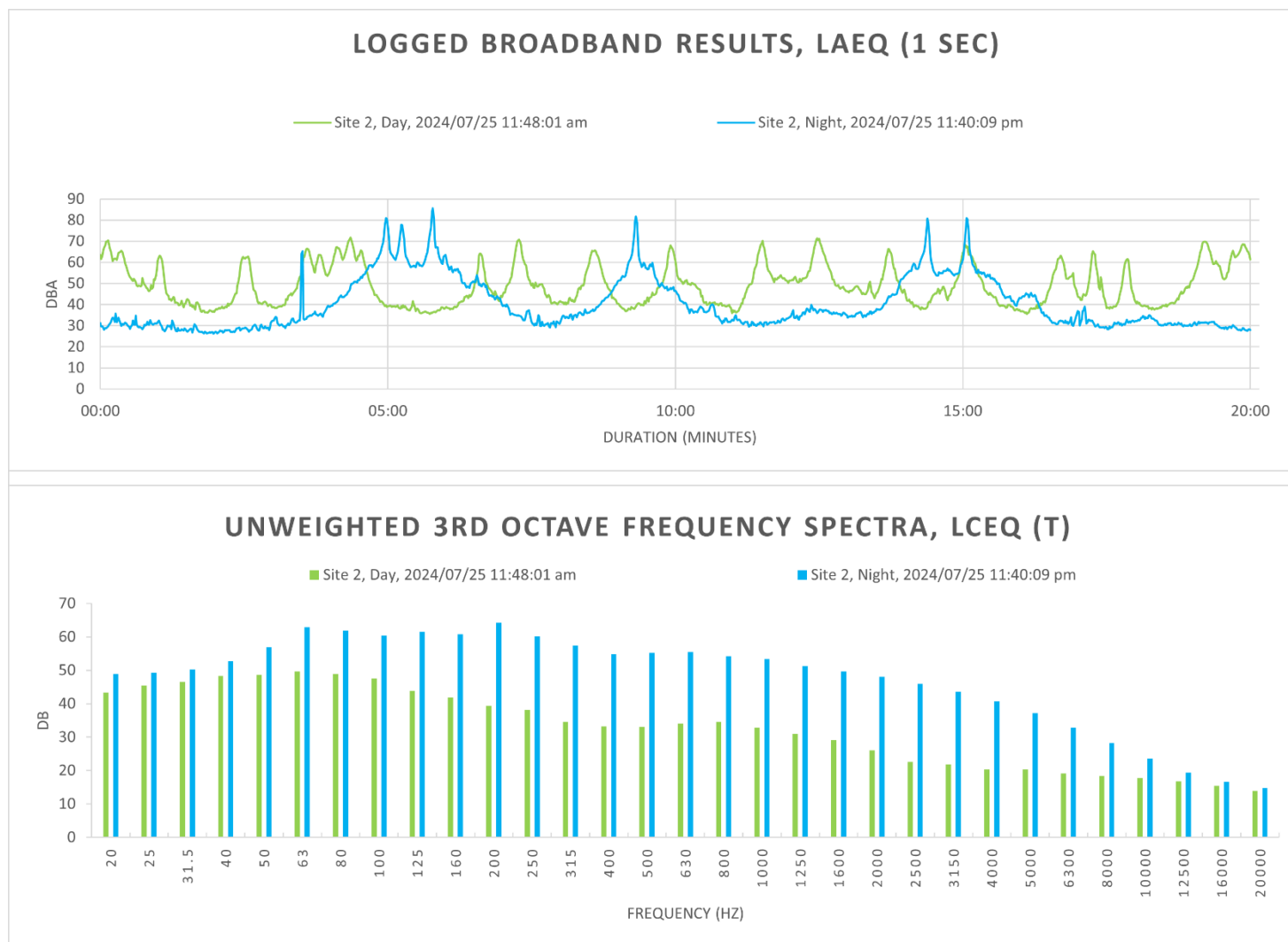


Figure D-2: Detailed day- and night-time survey results for Site 2

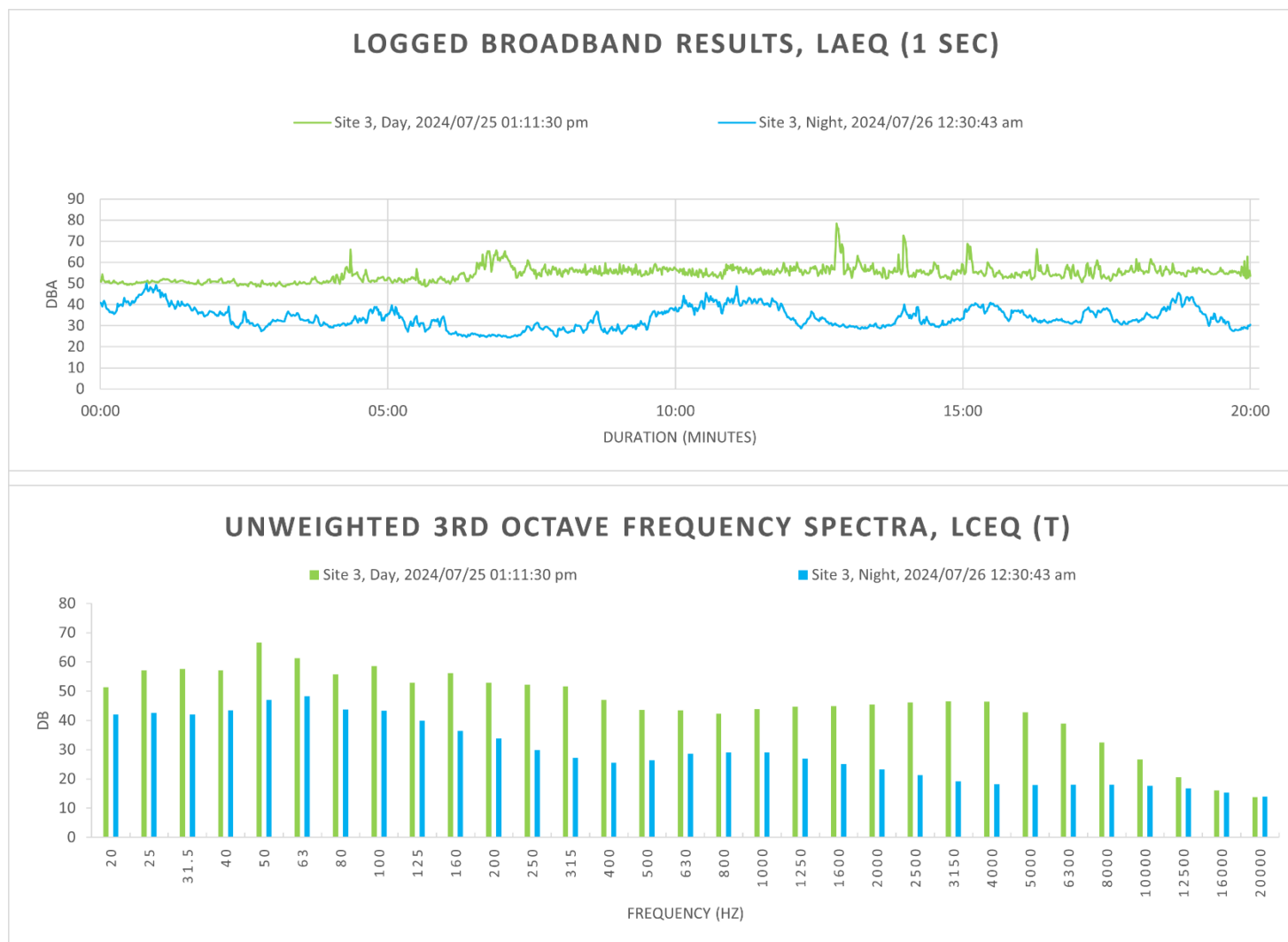


Figure D-3: Detailed day- and night-time survey results for Site 3

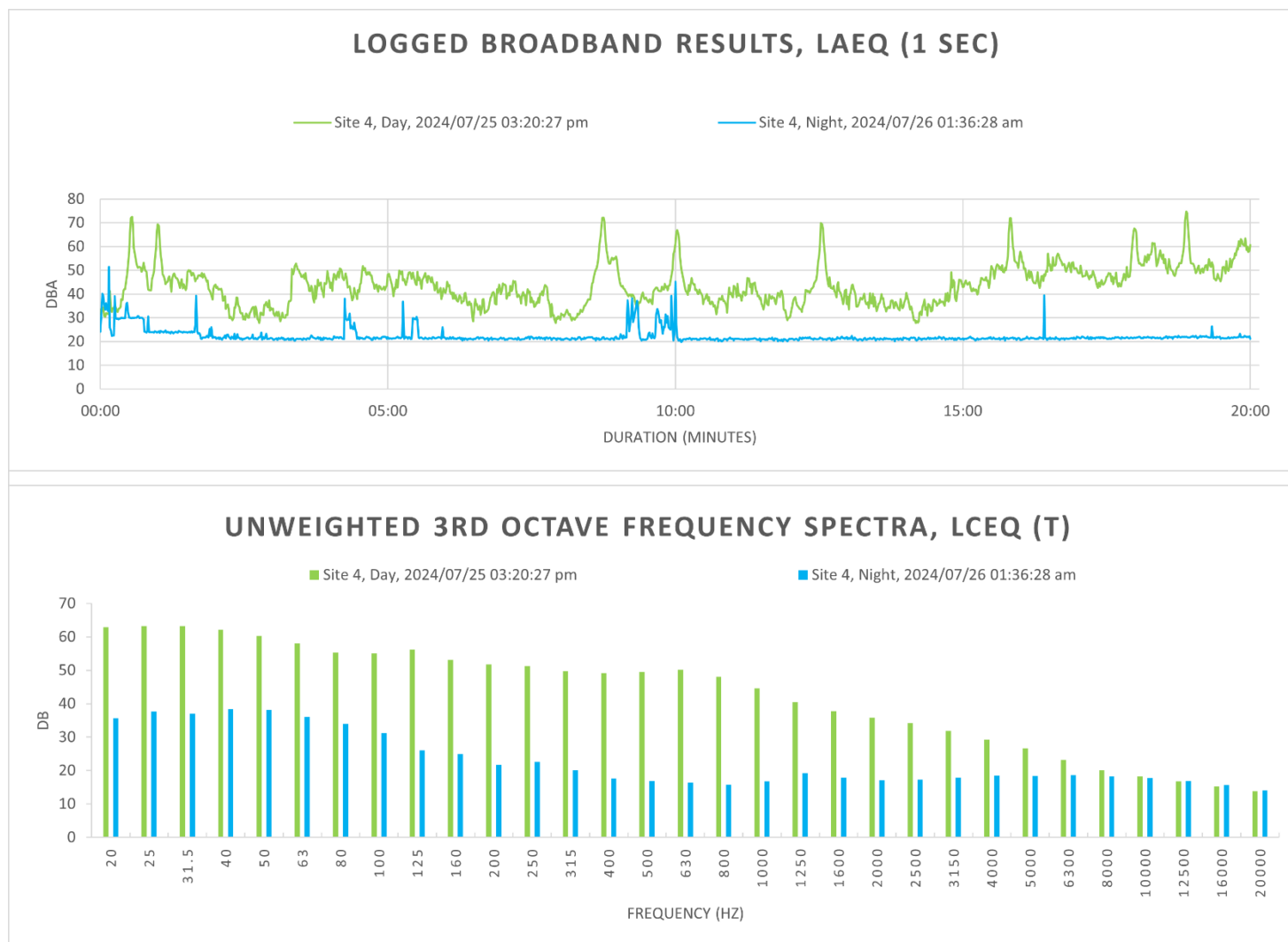


Figure D-4: Detailed day- and night-time survey results for Site 4

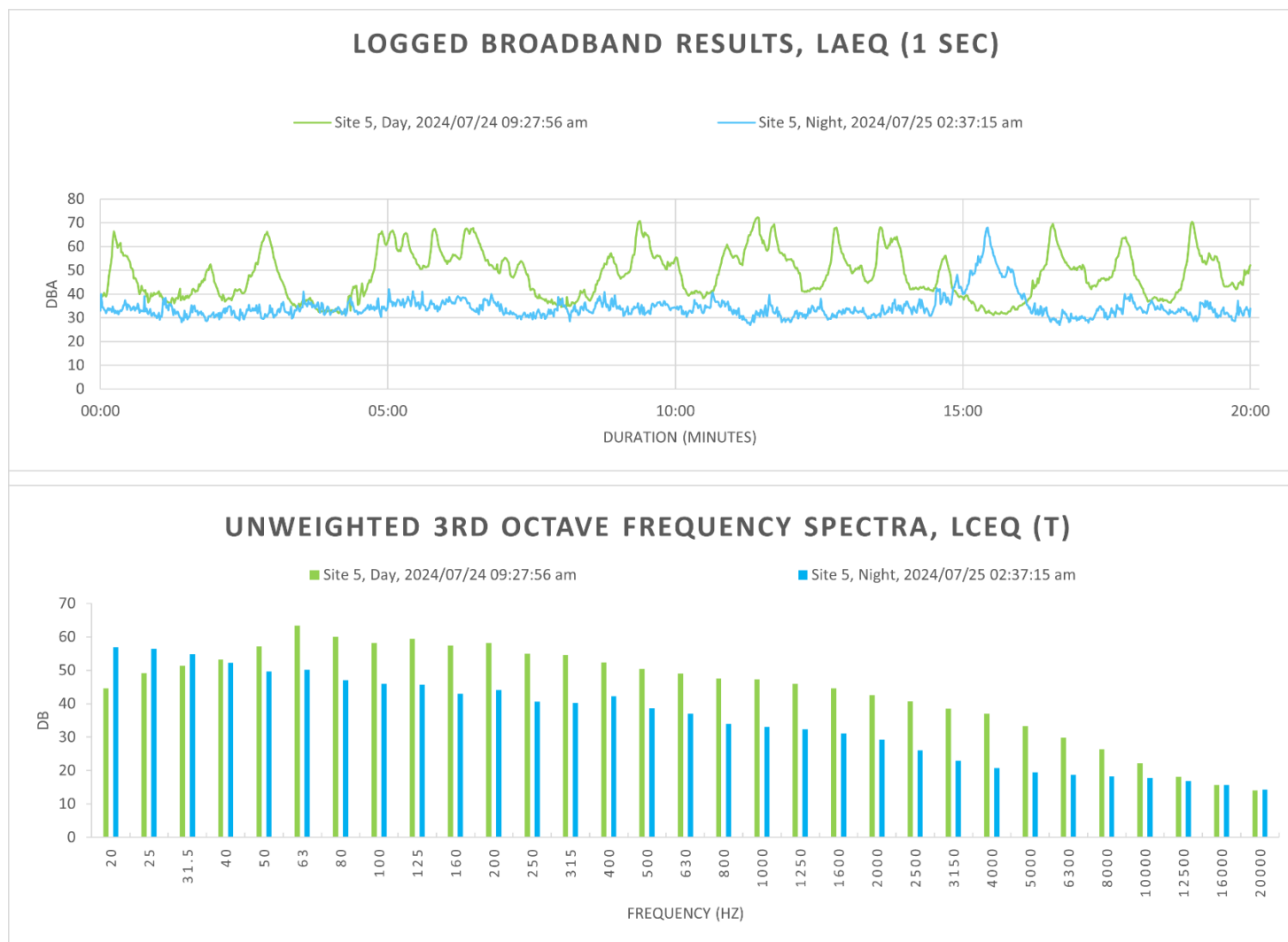


Figure D-5: Detailed day- and night-time survey results for Site 5

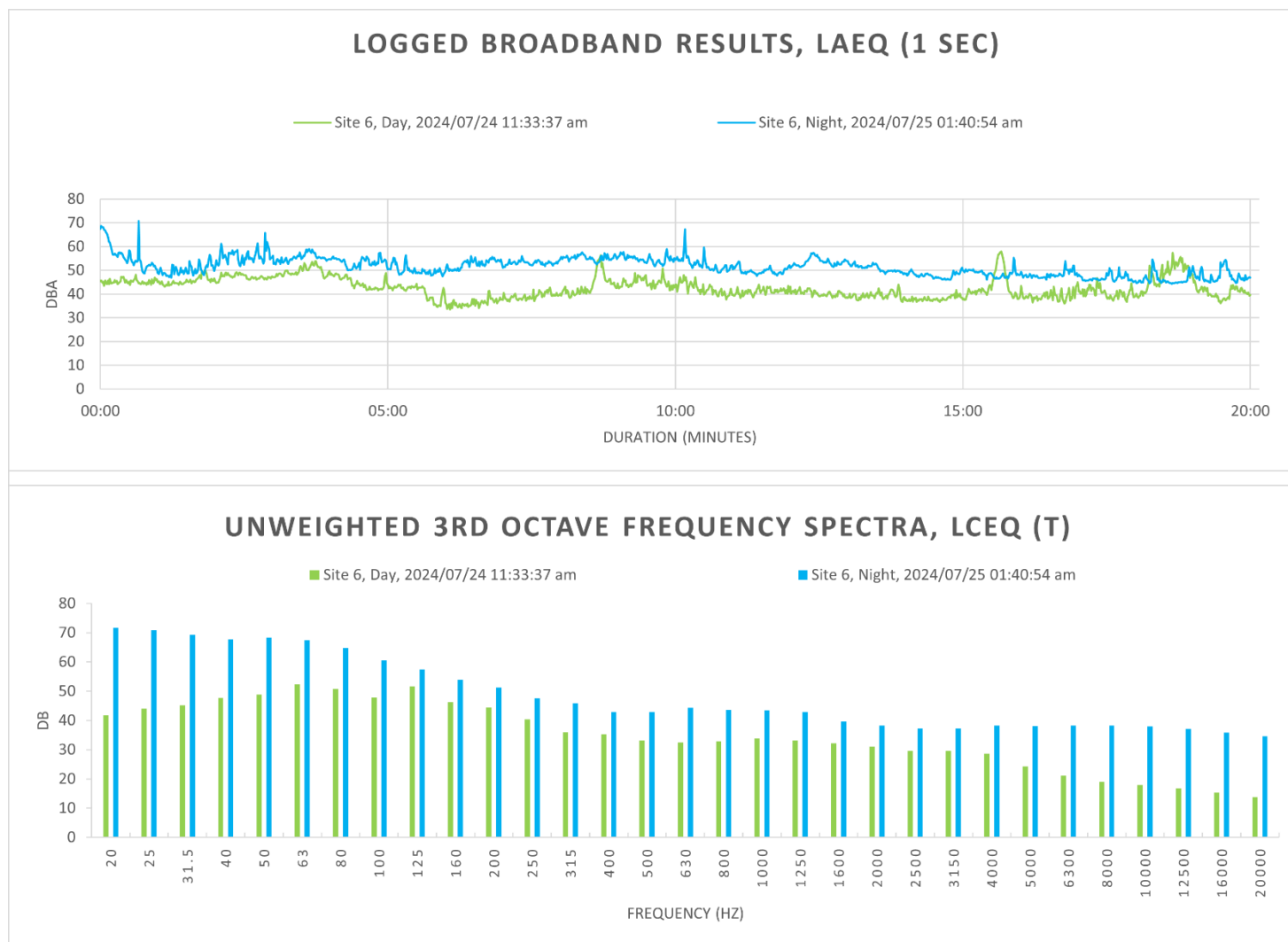


Figure D-6: Detailed day- and night-time survey results for Site 6

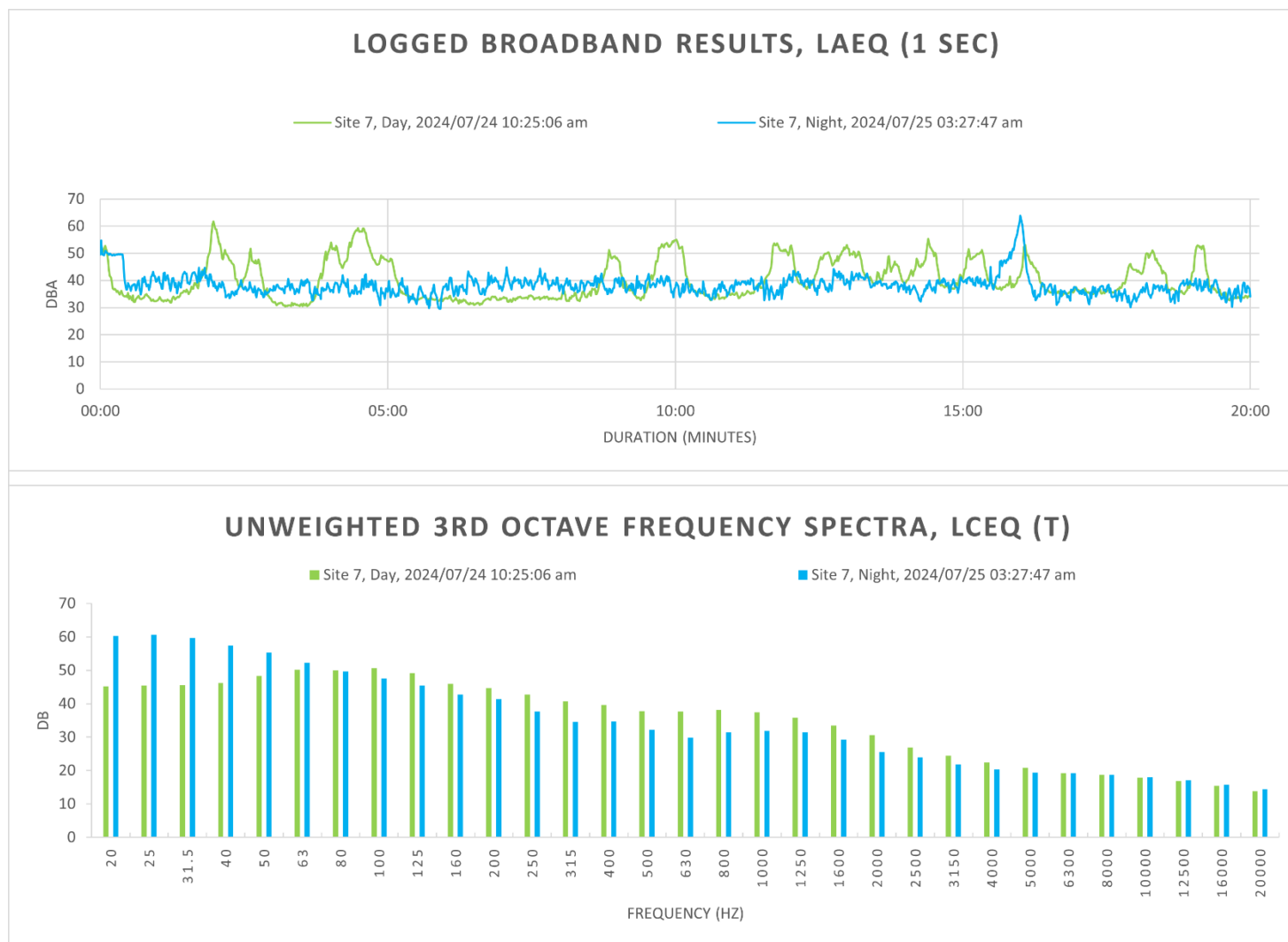


Figure D-7: Detailed day- and night-time survey results for Site 7

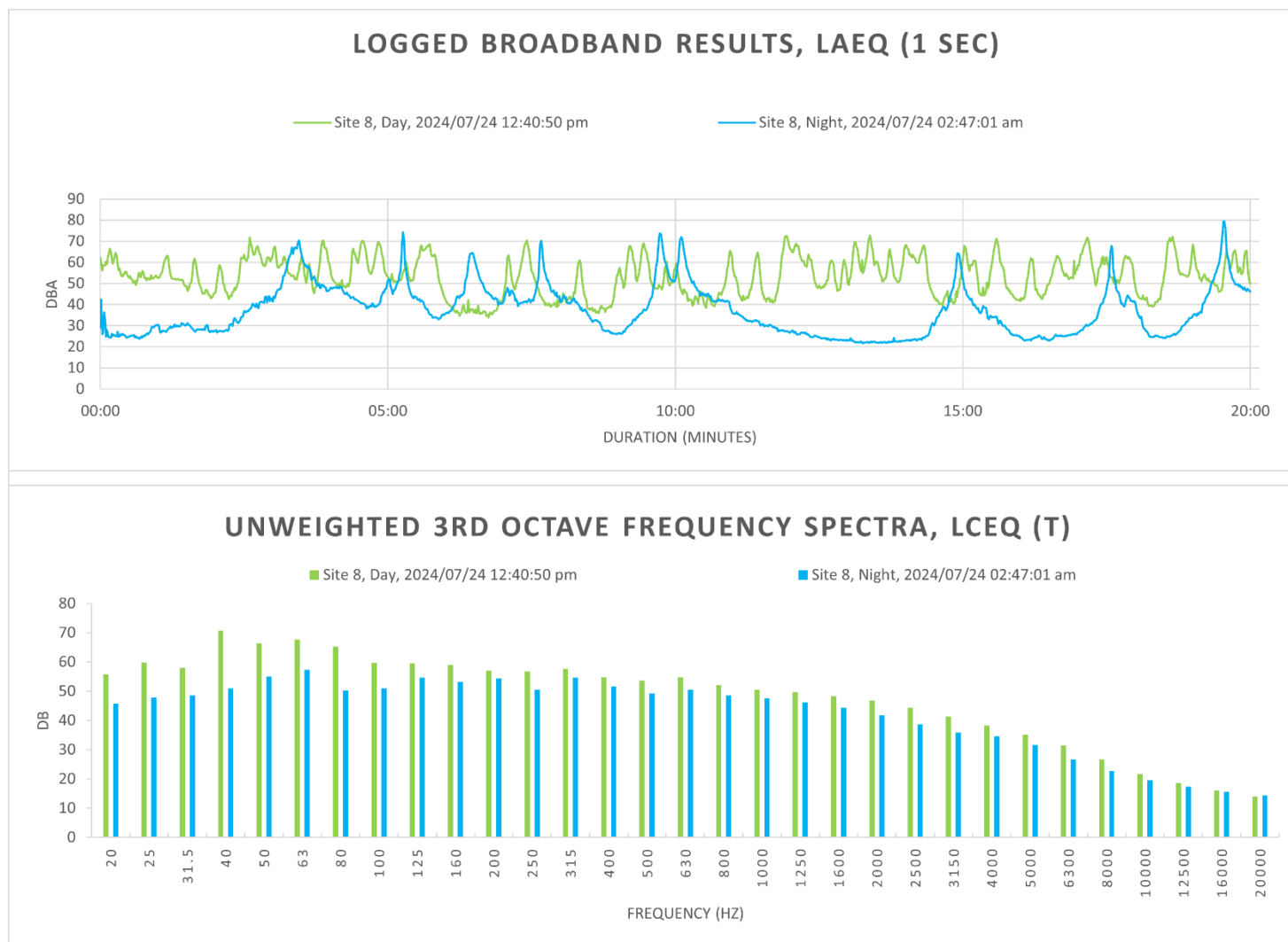


Figure D-8: Detailed day- and night-time survey results for Site 8

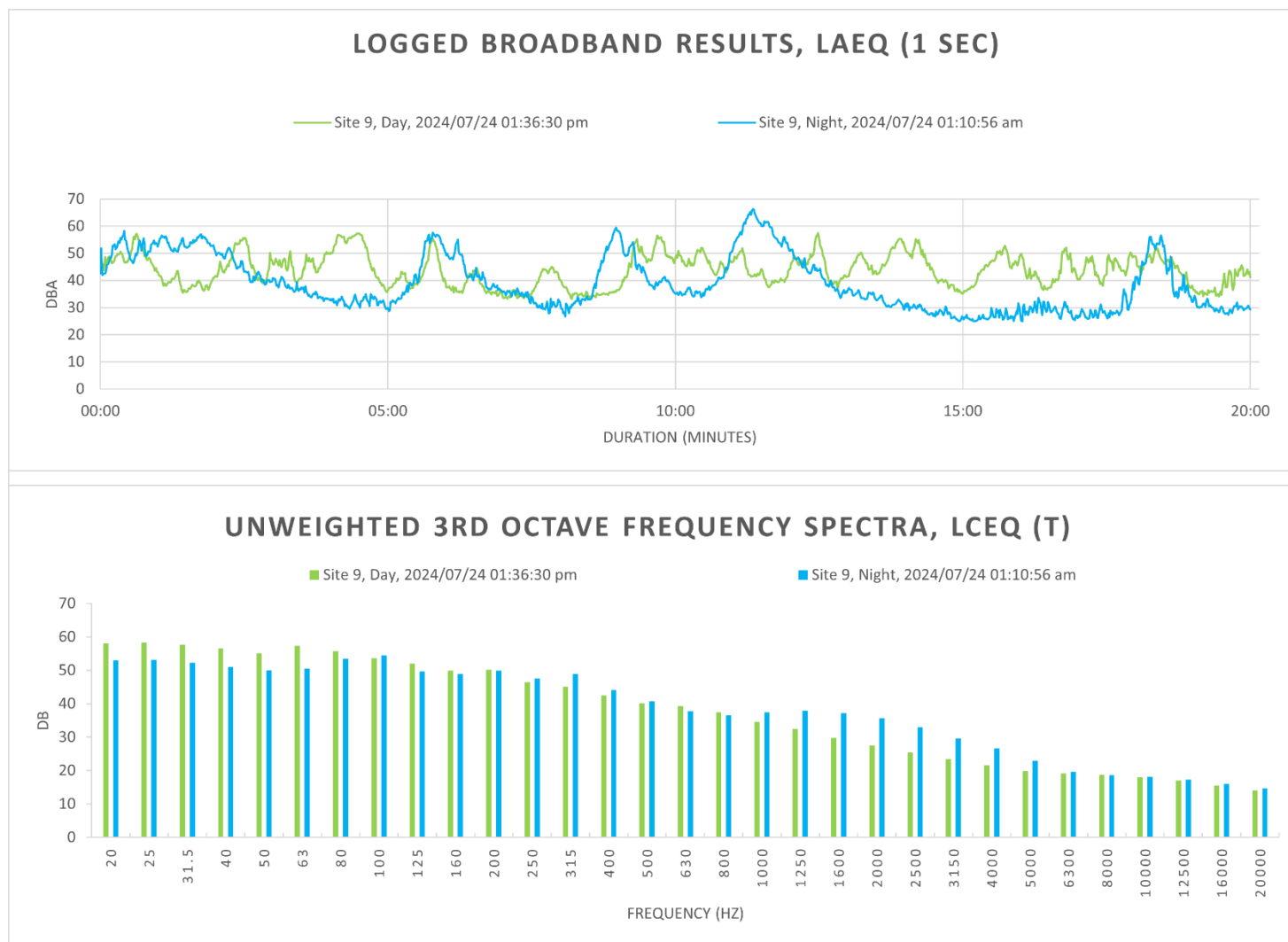


Figure D-9: Detailed day- and night-time survey results for Site 9

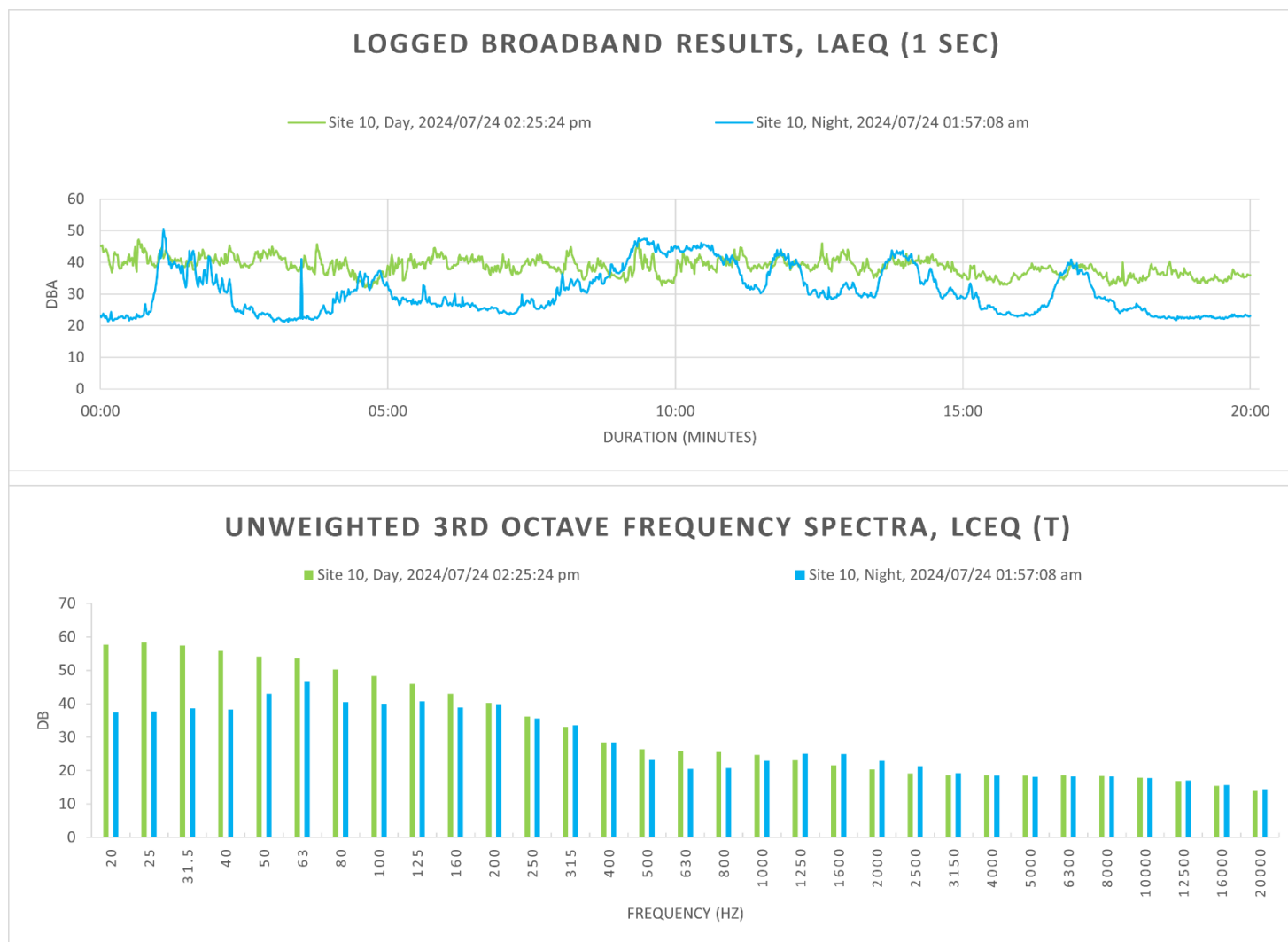


Figure D-10: Detailed day- and night-time survey results for Site 10

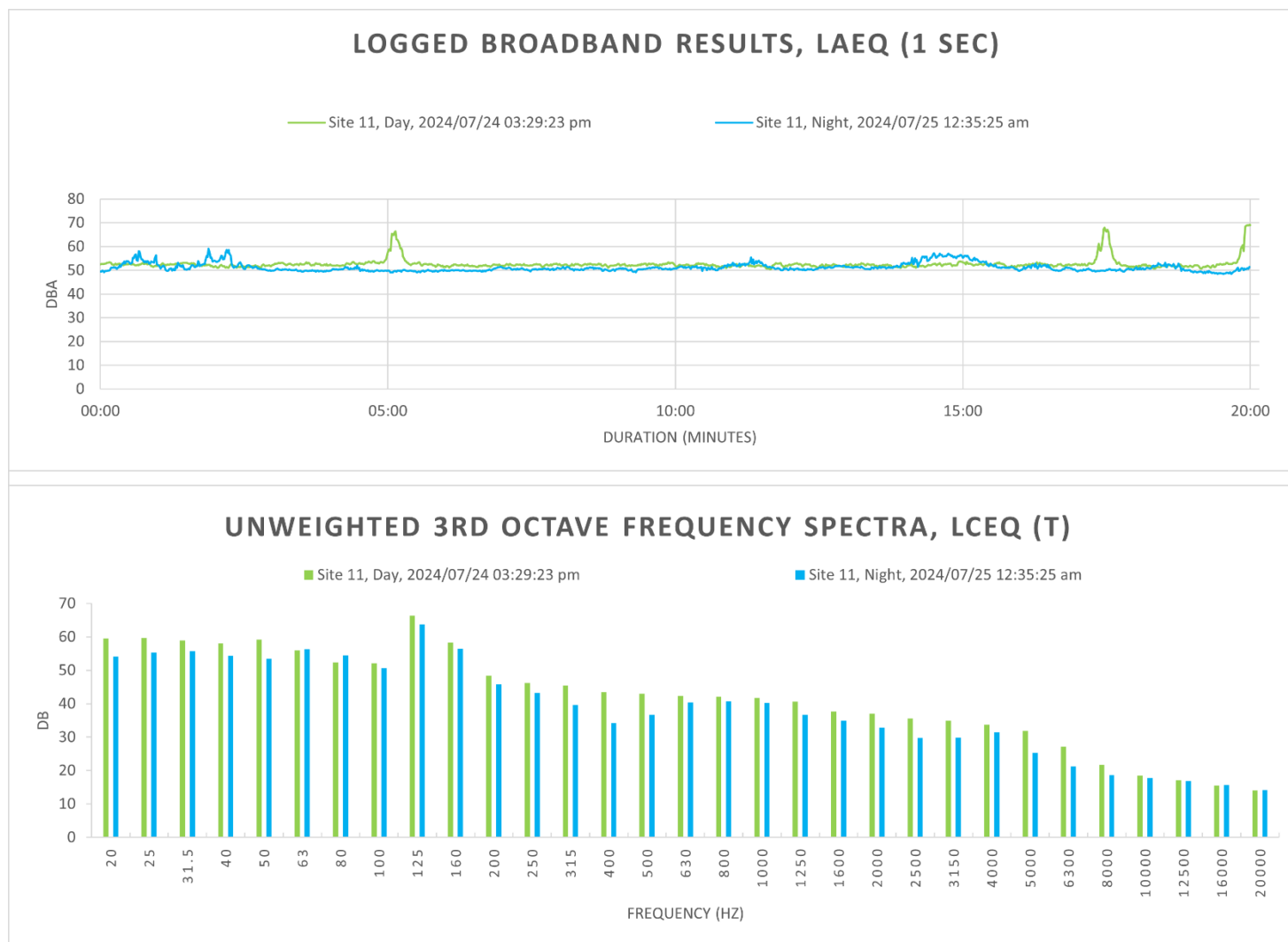


Figure D-11: Detailed day- and night-time survey results for Site 11

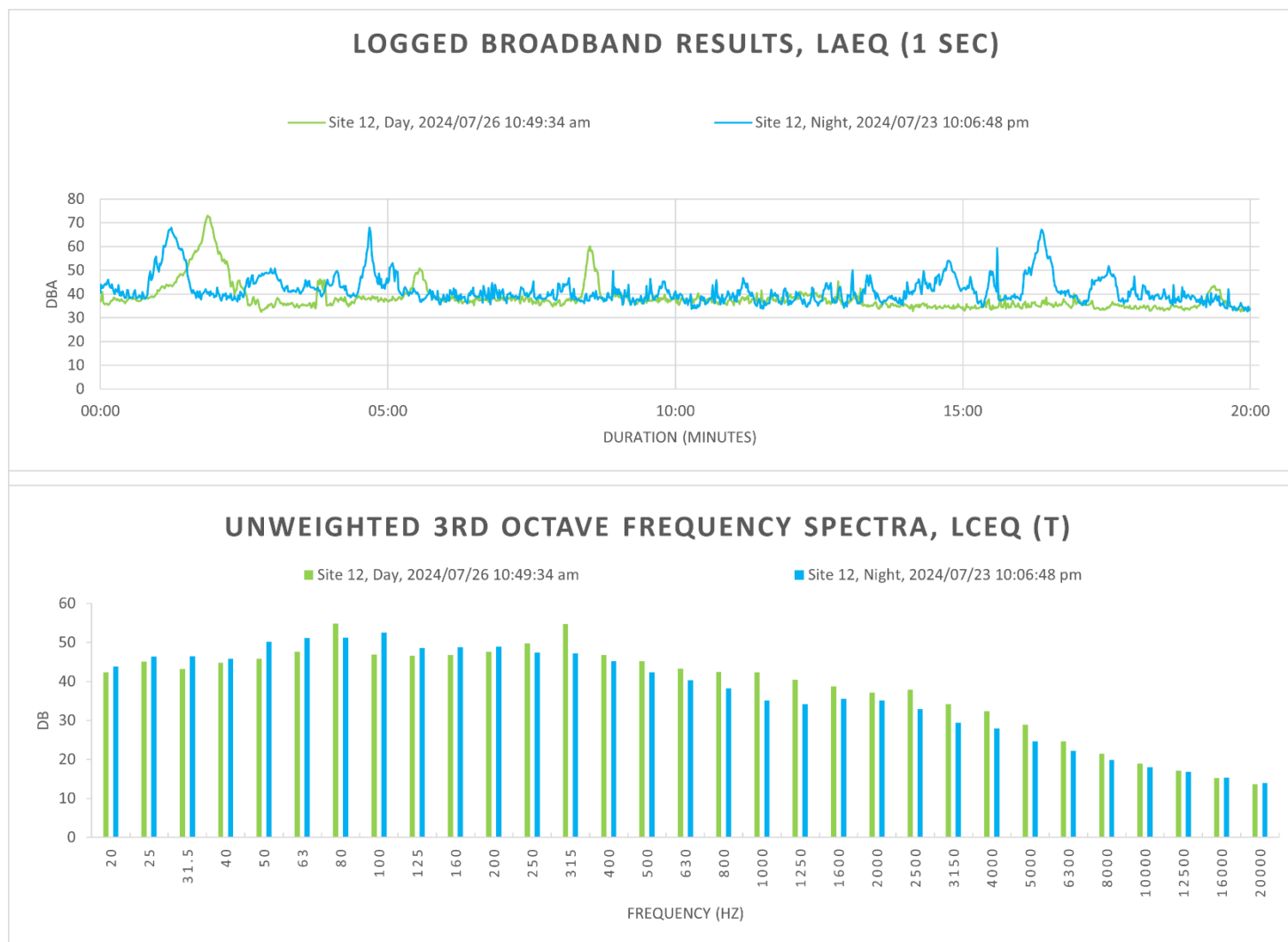


Figure D-12: Detailed day- and night-time survey results for Site 12